

Impact of Micromist in CNC Machining

Wayne Hung¹, Rufus Lamere², and Gary SanMiguel³

¹Texas A&M University, College Station, TX

²Texas State Technical College, Waco, TX

³Biomedical Manufacturing Center, Athens, TX

Contact: hung@tamu.edu

Present at
The Fourth Annual HTEC Conference
Detroit, Michigan
July 13-15, 2010

AGENDA

Impact of Micromist in CNC Machining



Source: furtech.typepad.com

- 1) Introduction
 - 2) Objectives
 - 3) NSF-RET program
 - 4) Investigation
 - Cutting fluids
 - Micromist
 - Machinability
 - 5) Summary
 - 6) Future works
- Acknowledgement
- References

INTRODUCTION

- ❑ The cost of cutting fluids is around 17% of the machining costs of automotive components.
- ❑ 1.2 million workers are affected by the chronic effects produced by cutting fluids.
- ❑ OSHA demands tighter control on cutting fluids (cost, maintenance, disposal, emission standards...)
- ❑ Propose solution: use micromist as minimum quantity lubrication in machining

OBJECTIVES

- 1) Characterize micromist
- 2) Apply micromist in macro/micro machining
- 3) Identify technical issues
- 4) Study economics of micromist

NSF-RET program

- 1) Is funded by National Science Foundation
- 2) Provides research experience to teachers /instructors from nearby high schools /community colleges.
- 3) Covers 9 weeks in summer
- 4) Must implement to home institutions

NSF-RET program (summer2010)

- ❑ Rufus Lamere, Texas State Technical College, Waco, TX
- ❑ Gary Miguel, Biomedical Manufacturing Center, Athens, TX
- ❑ Wayne Hung, Texas A&M University, College Station, TX



INVESTIGATION: setup

- 1) Machines: Haas OM2 CNC micromill, VF1 CNC mill, and SL20 CNC lathe.
- 2) Workpieces:
 - Micromachining: 12 mm (1/2 in) square bars of 316L stainless steel, CP titanium PEEK plastics, H11 tool steel, 1010 steel, 6061-T6 aluminum.
 - Macromachining: 4140 steel bars / plates
- 3) Tools
 - Micromill: TiN un/coated WC, Ø100-1016µm (0.004-0.040 in)
 - Microdrill: Uncoated WC Ø50-203µm (0.002-0.008 in)
 - Macromill: TiN un/coated WC Ingersoll APKT102308R-HS insert, Ø15.8 (5/8 in)
 - Macroface: TiN un/coated WC Hertel TNG431 insert
- 4) Tool failure criteria: 50 µm (0.002 in) flank wear for microtool, 300 µm (0.012 in) for macrotool.

INVESTIGATION: setup

5) Machining parameters:

- Micromilling: 15-157 m/min (50-520 ft/min), 10 μm /tooth (0.0004 in/tooth), 0.35mm (0.014 in) axial depth, 0.56 mm (0.022 in) radial depth, climb (down) side milling.
- Macromilling: 55-102 m/min (183-343 ft/min), 0.043-0.178 mm/tooth (0.0017-.0070 in/tooth), 1-2 mm (0.04-0.08 in) axial depth, 4.25-8.5 mm (0.17-0.333 in) radial depth, down milling on D2 tool steel.
- Macrofacing: max 44-80 m/min (147-265 ft/min), 0.5 mm (0.020 in) depth of cut, 0.1-0.3 mm/rev (0.004-0.006 in/rev) feedrate, constant RPM, on 4140 steel.

6) Cutting fluids:

- Dry
- Flood cooling: synthetic Blasocut 2000 Universal, 5:1 mixture
- Micromist: UNIST Uni-MAX system, 2210EP oil, 0.022 cc/min. Use with Mistbuster500.

INVESTIGATION: setup

7) Measurement:

- Keyence LK-G82 laser system, 70 μ m beam, 50 kHz sampling rate, 0.2 μ m resolution
- Olympus STM6 measurement microscope, 0.1 μ m resolution
- JEOL JSM 6400 scanning electron microscope
- Video tensiometer FTA 188, 001 mN/m accuracy

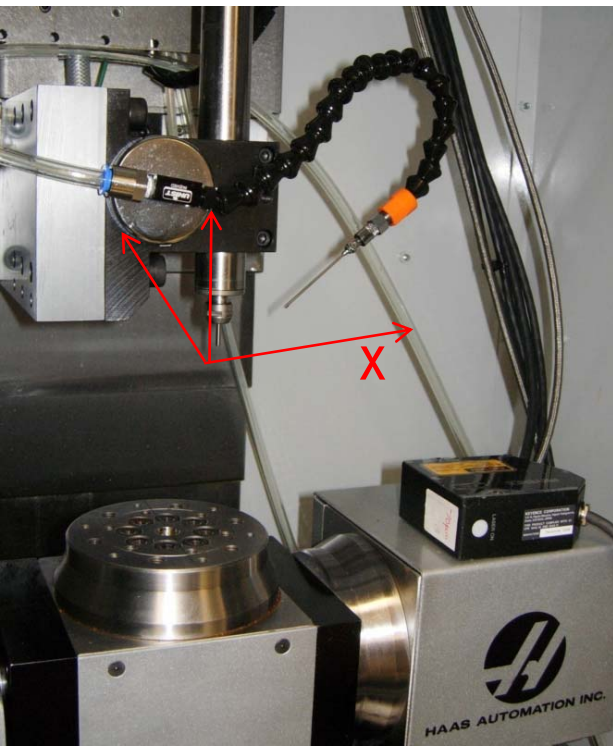
8) Computer aided tools

- SolidWorks, FeatureCam, and MasterCam software
- Cosmos finite element software

INVESTIGATION: machines

Haas OM2 CNC micromill:

- 5-axis capability
- 50,000 rpm air spindle
- $\pm 1 \mu\text{m}$ spindle runout
- $\pm 3 \mu\text{m}$ repeatability

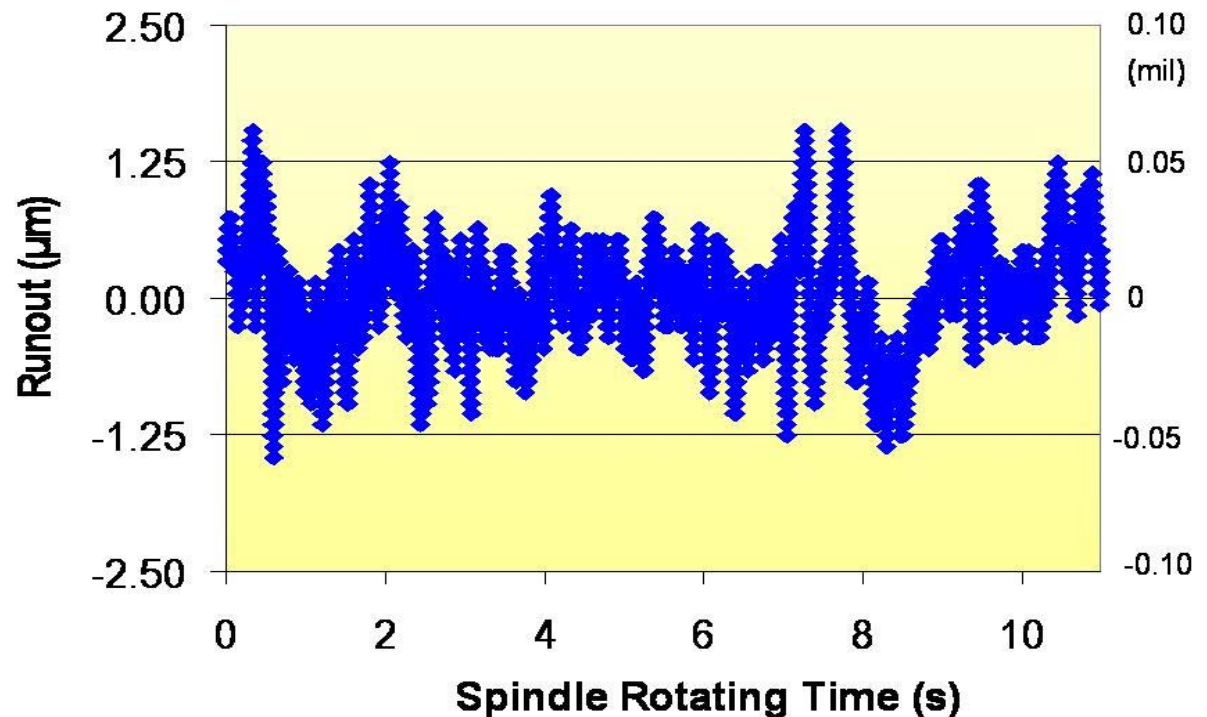


Micromist

- 2210EP oil, 0.022 cc/min
- 30 mm @ 60° from z axis
- -45° in x-y plane

Spindle Runout: Laser on Haas OM2

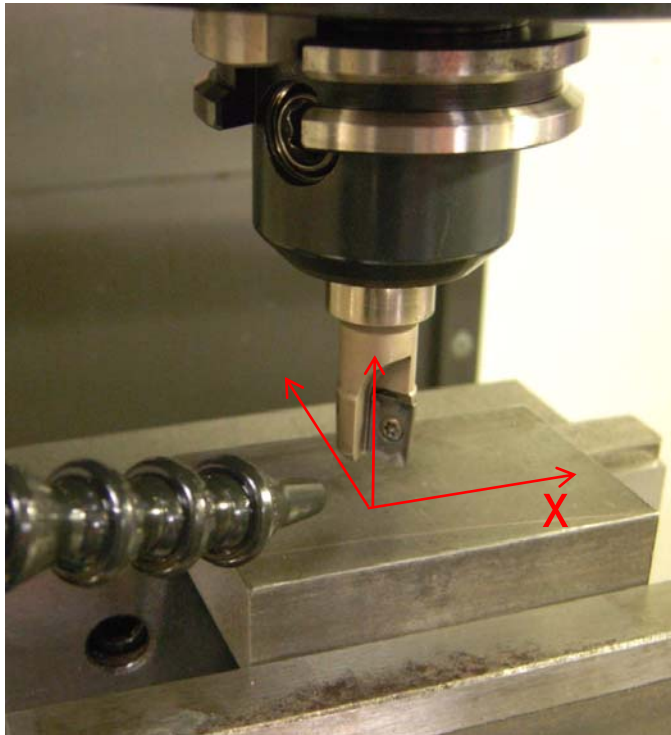
$\varnothing 3\text{mm}$ (1/8") plug gage @ 10k rpm



INVESTIGATION: machines

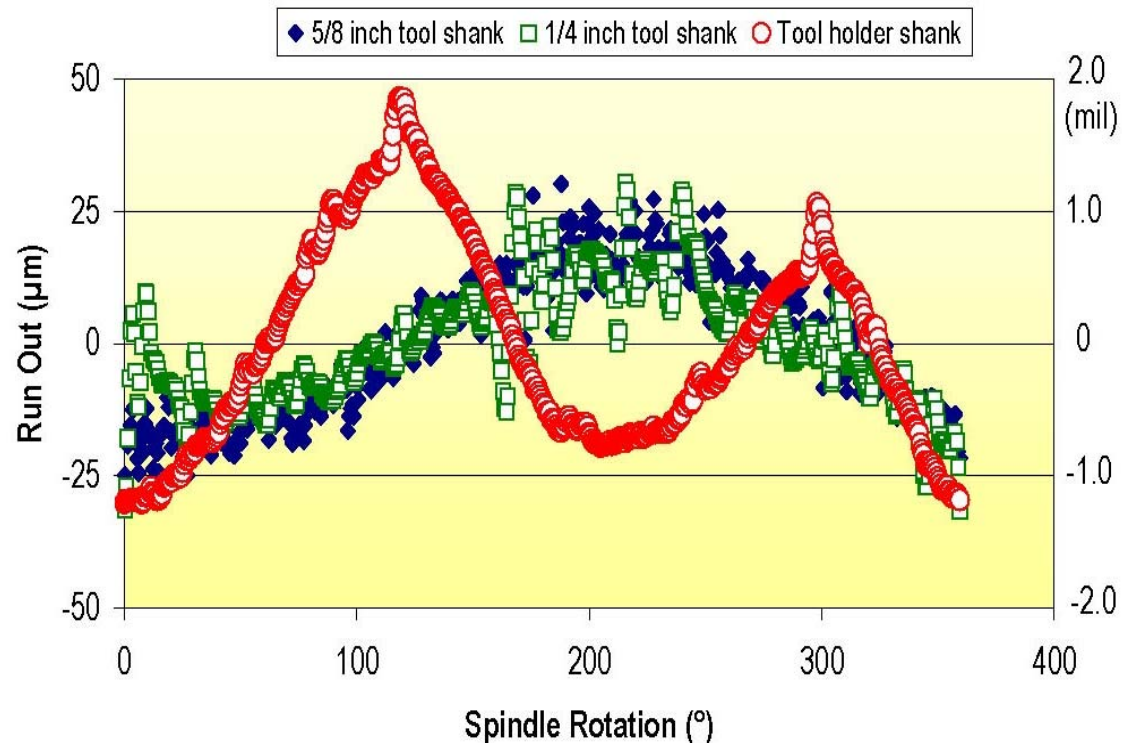
Haas VF1 CNC mill:

- 5-axis capability
- 7,500 rpm spindle
- $\pm 25 \mu\text{m}$ spindle runout
- $\pm 3 \mu\text{m}$ repeatability



Micromist

- 2210EP oil, 0.022 cc/min
- 25 mm @ 70° from z axis
- -120° in x-y plane



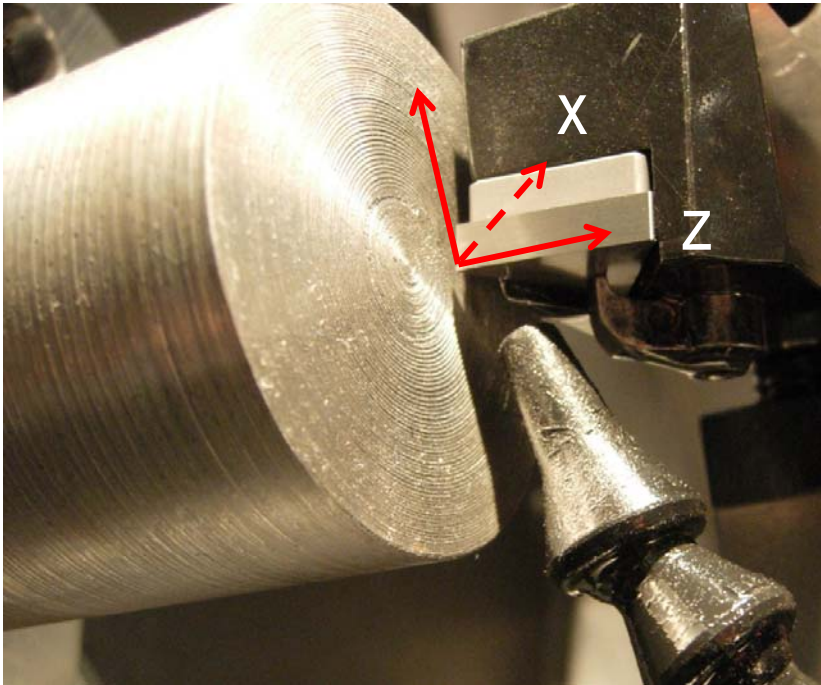
INVESTIGATION: machines

Haas SL20 CNC lathe:

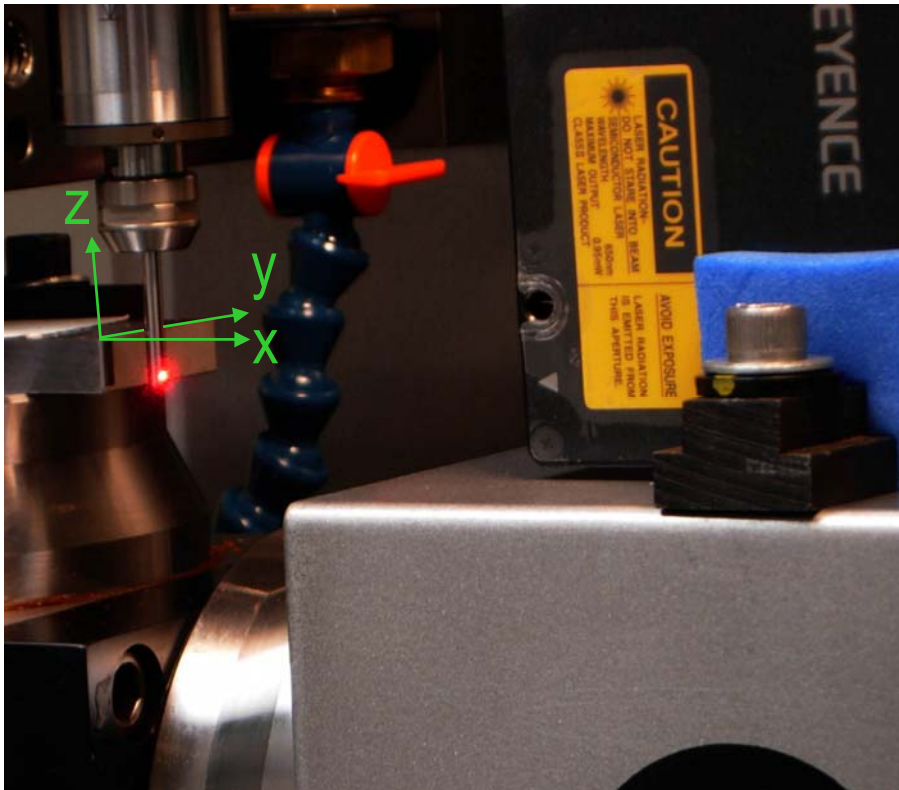
- Live tooling capability
- 3,400 rpm spindle
- $\pm 3 \mu\text{m}$ repeatability

Micromist

- 2210EP oil, 0.022 cc/min
- 6 mm @ 150° from y axis
- -60° in x-y plane

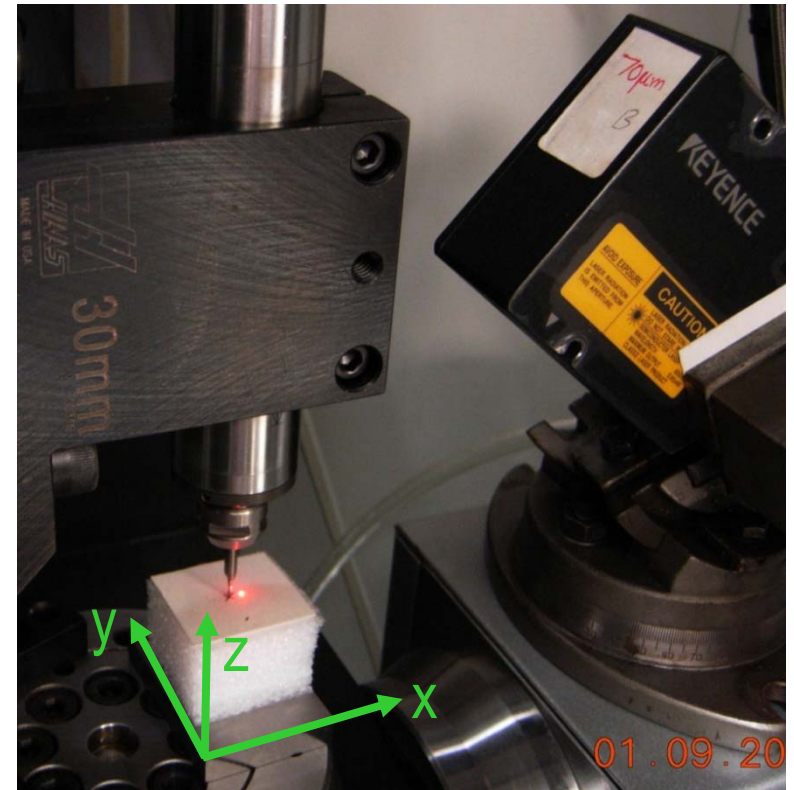


MICROMACHINING: tool setting



(a)

Set up for edge detection on x-y plane

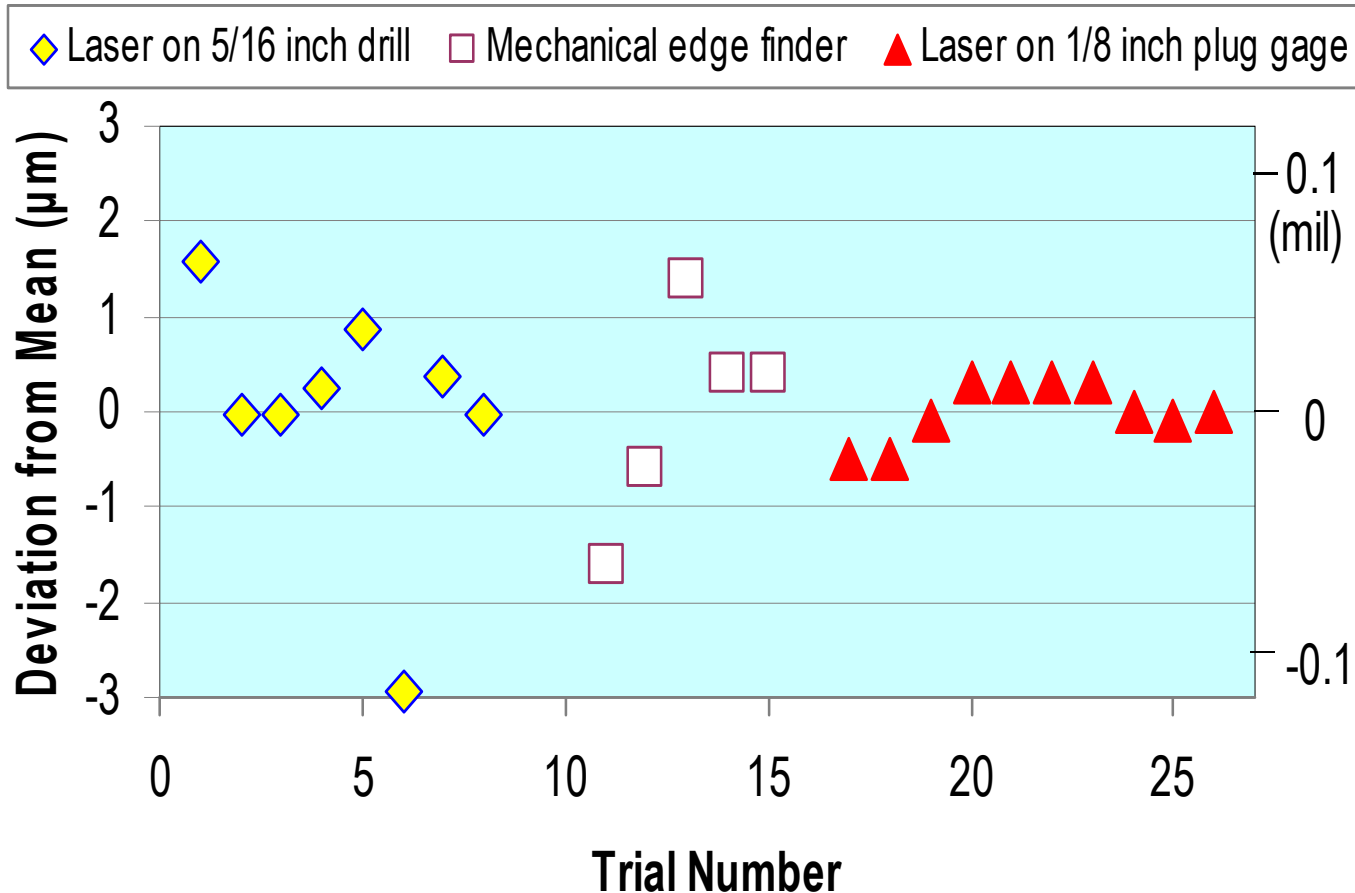


(b)

Set up for tool height z-offset

Microtool offset using laser sensor

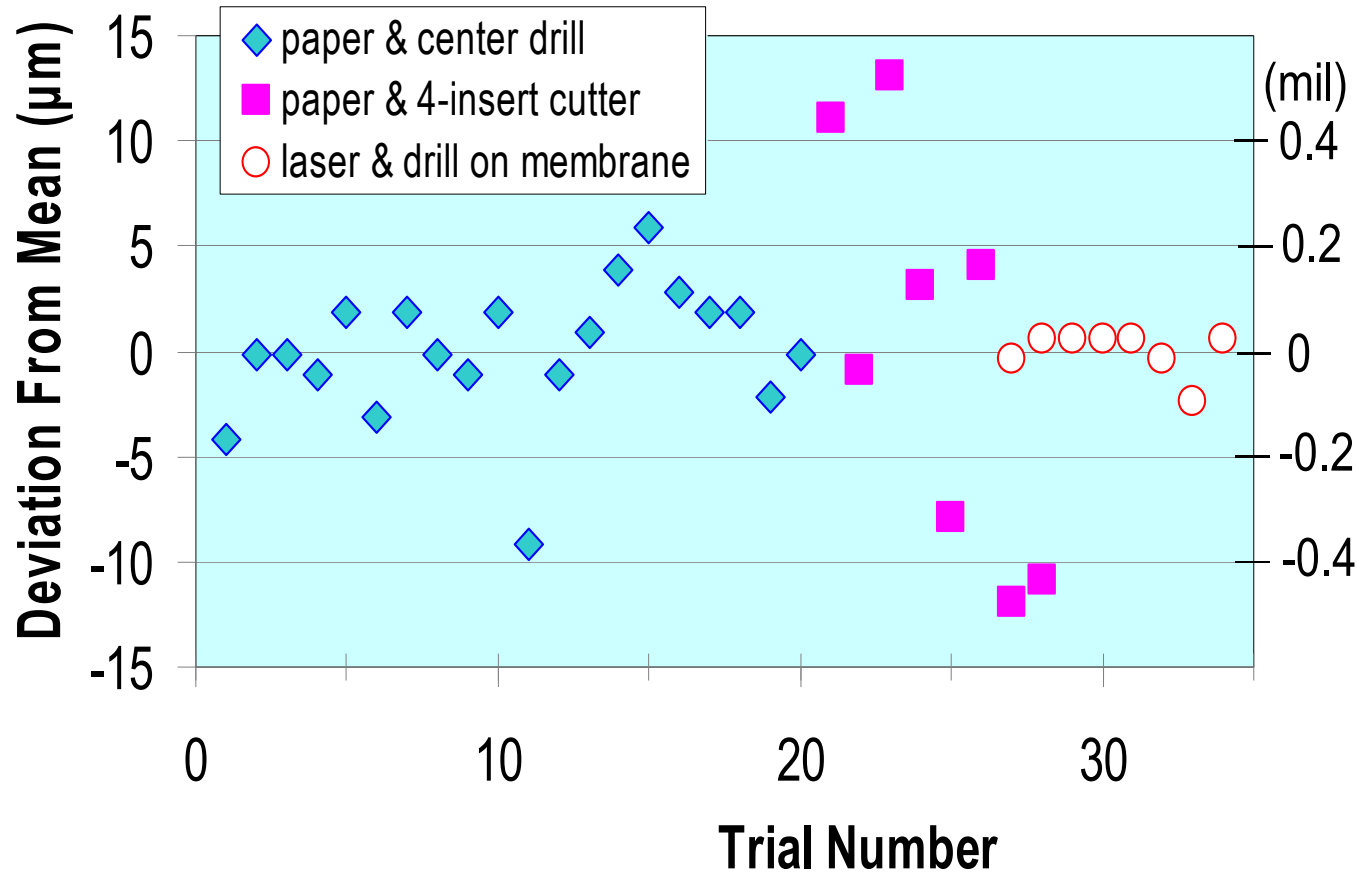
MICROMACHINING: tool setting



- X, Y settings depend on tool quality
- A precision plug gage should be used

Edge detection for tool offsets in x, y directions.

MICROMACHINING: tool setting



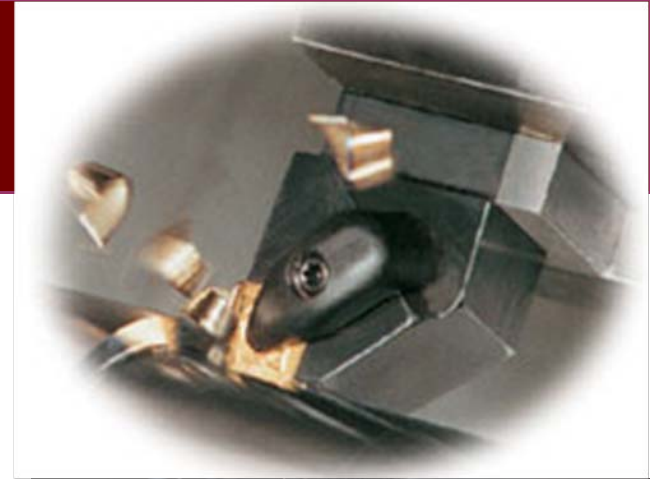
- Z offset depends on tool geometry
- Expect a larger z offset error than x, y offsets

Tool height offset in z direction.

MACHINING: cutting fluid

For effective cooling/lubricating, cutting fluid must:

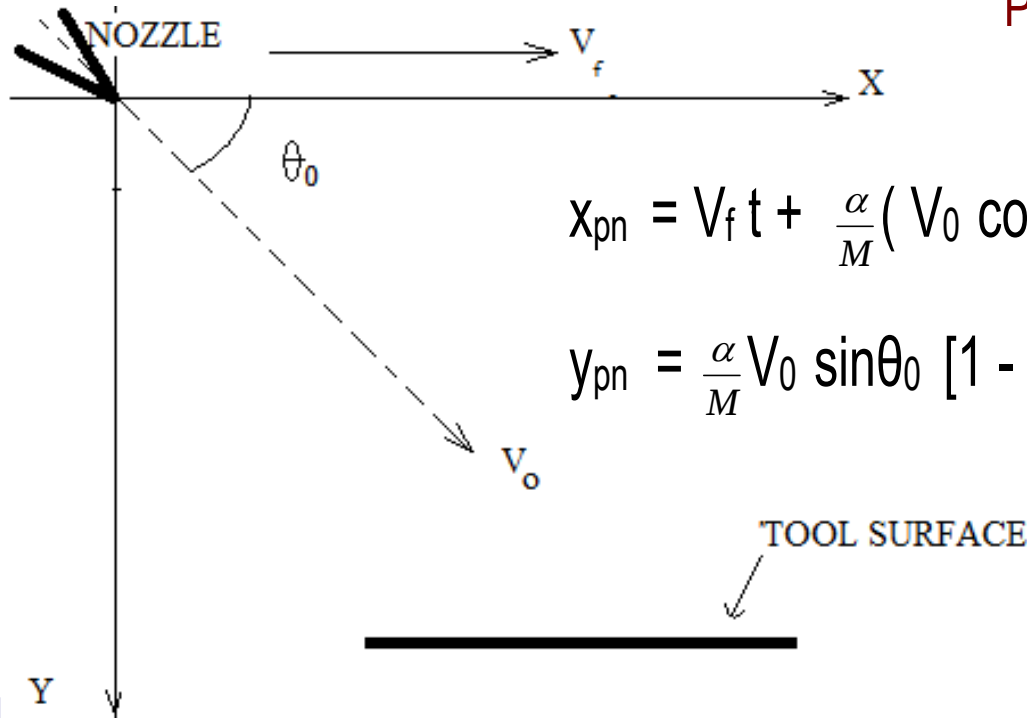
- 1) Penetrate the boundary layer of a rapidly rotating tool,
- 2) Adhere to a tool surface despite centrifugal force, and
- 3) Wet the tool/chip interface to provide lubricating/cooling





MACHINING: micromist

Particle Trajectory



Penetrate?

Particle trajectory

CFD modeling

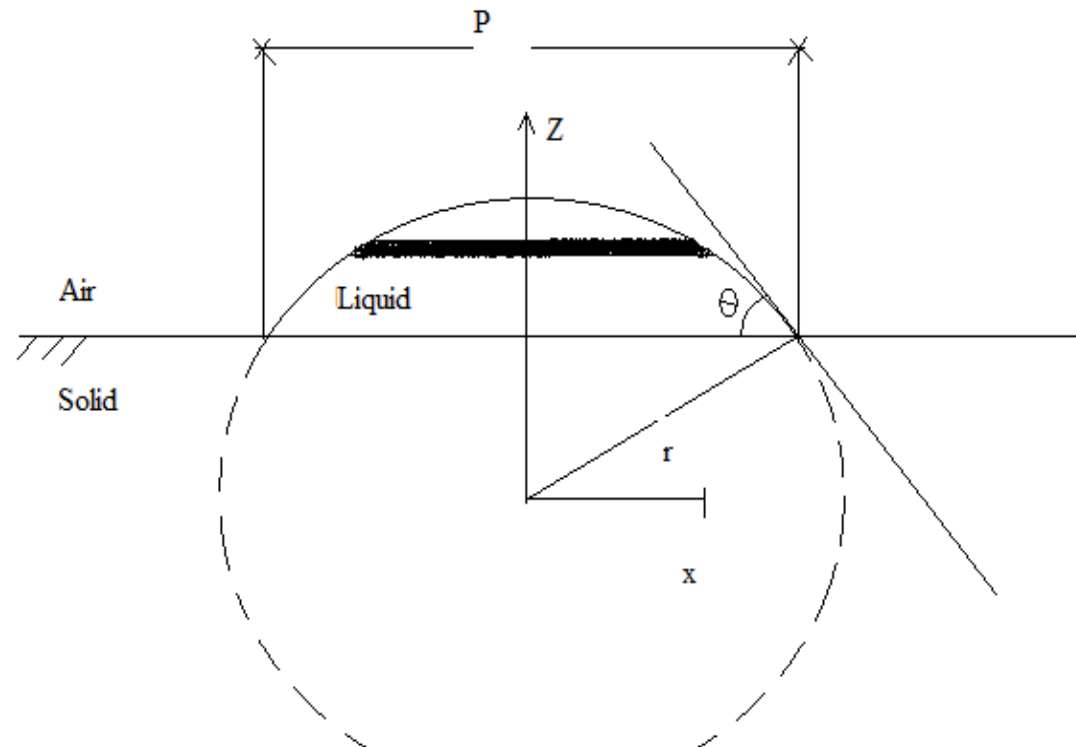
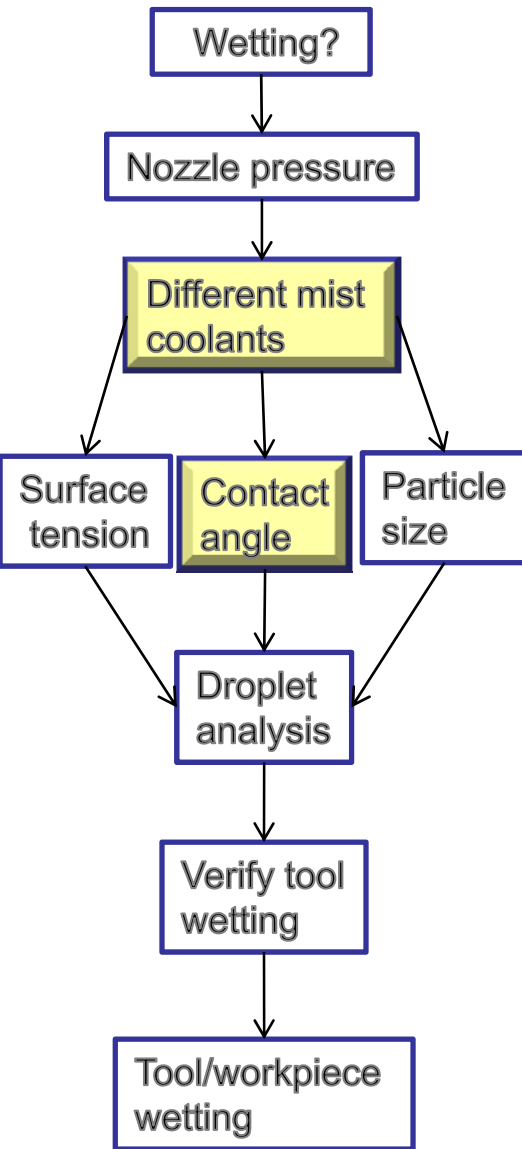
Optimal tool/workpiece/
nozzle positions

$$x_{pn} = V_f t + \frac{\alpha}{M} (V_0 \cos \theta_0 - V_f) [1 - e^{-(\alpha/M)t}]$$

$$y_{pn} = \frac{\alpha}{M} V_0 \sin \theta_0 [1 - e^{-(\alpha/M)t}]$$

TOOL SURFACE

MACHINING: coolant wetting



$$\frac{P}{V^{1/3}}(\theta) = \left[\frac{24}{\pi} \cdot \frac{(1 - K \cos^2 \theta)^{3/2}}{2 - 3 \cos \theta + \cos^3 \theta} \right]^{1/3}$$

V: volume of droplet

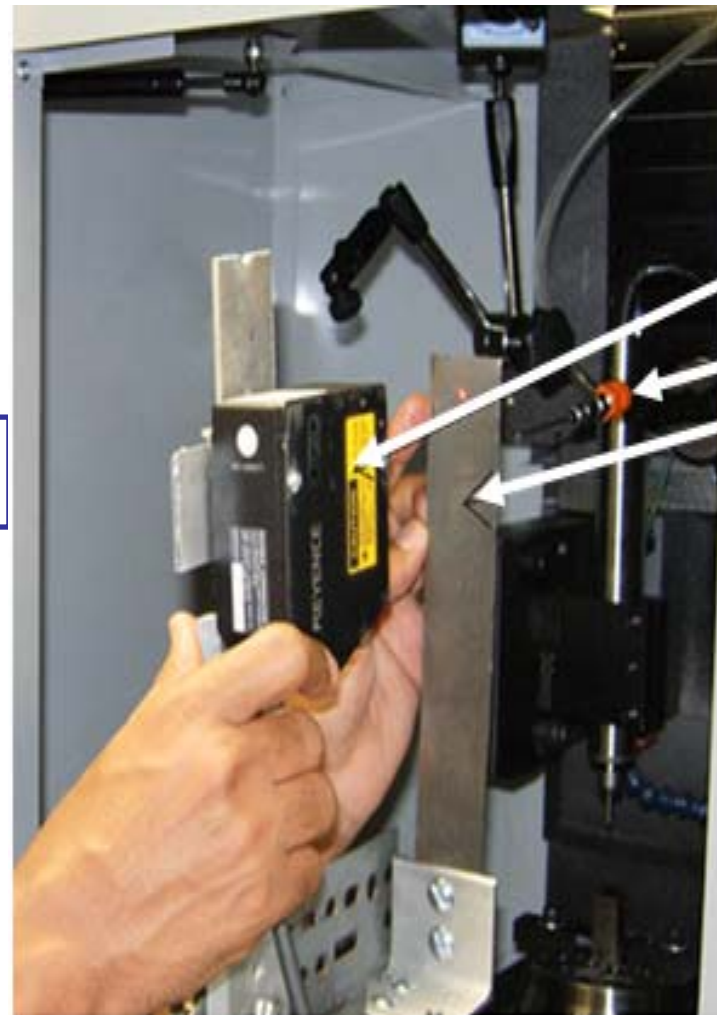
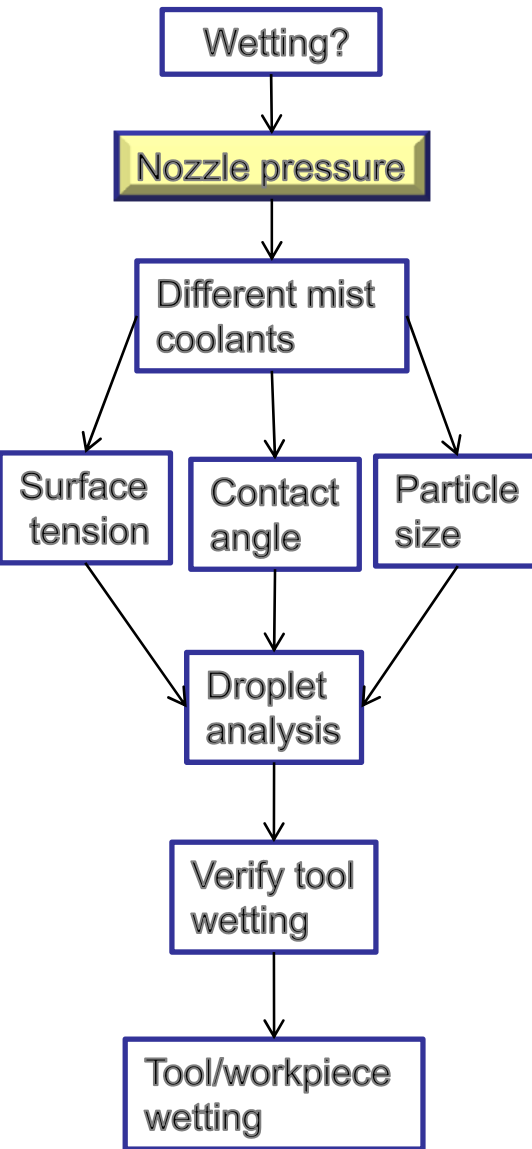
P: diameter of droplet

K: 1 for $\theta < 90^\circ$; 0 for $\theta > 90^\circ$

θ : contact angle



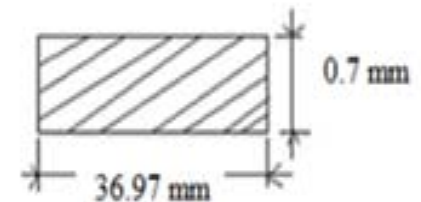
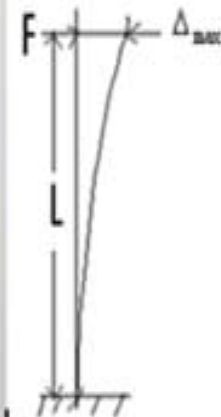
MACHINING: micromist



Laser displacement sensor

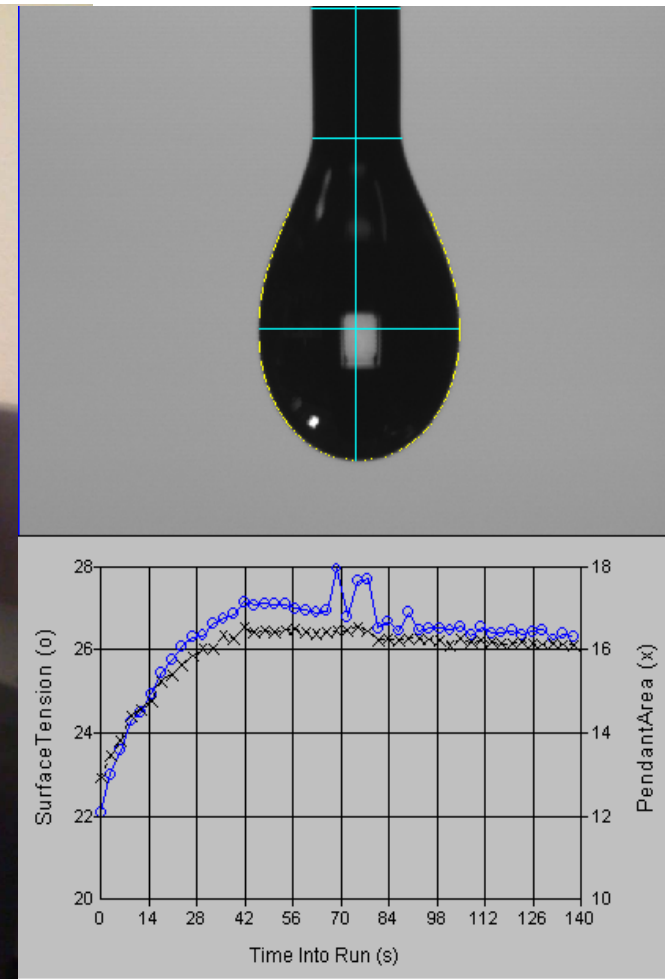
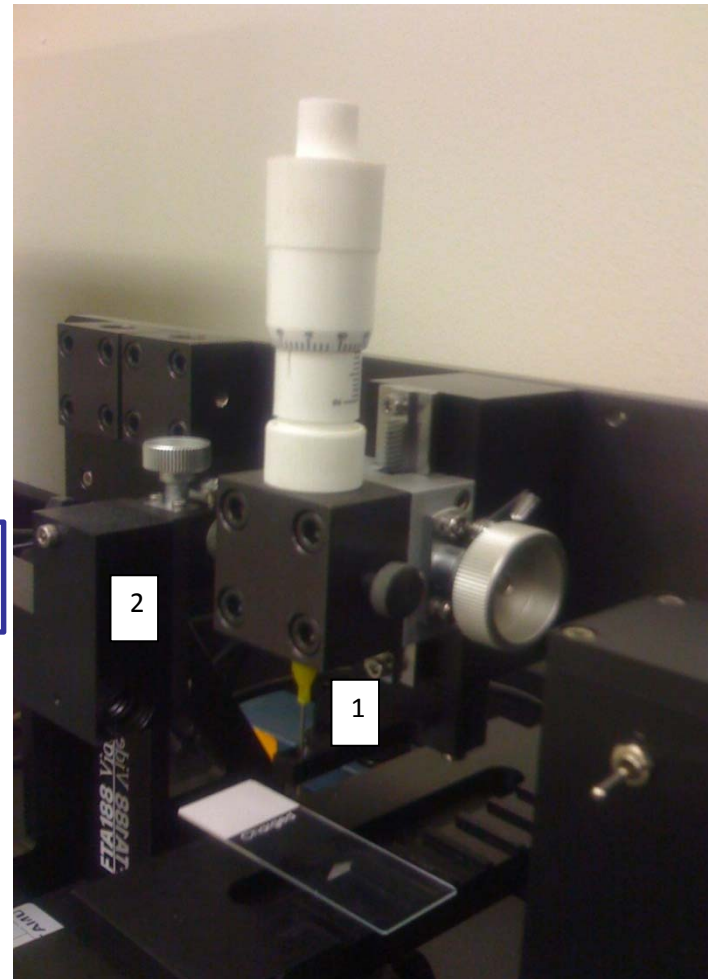
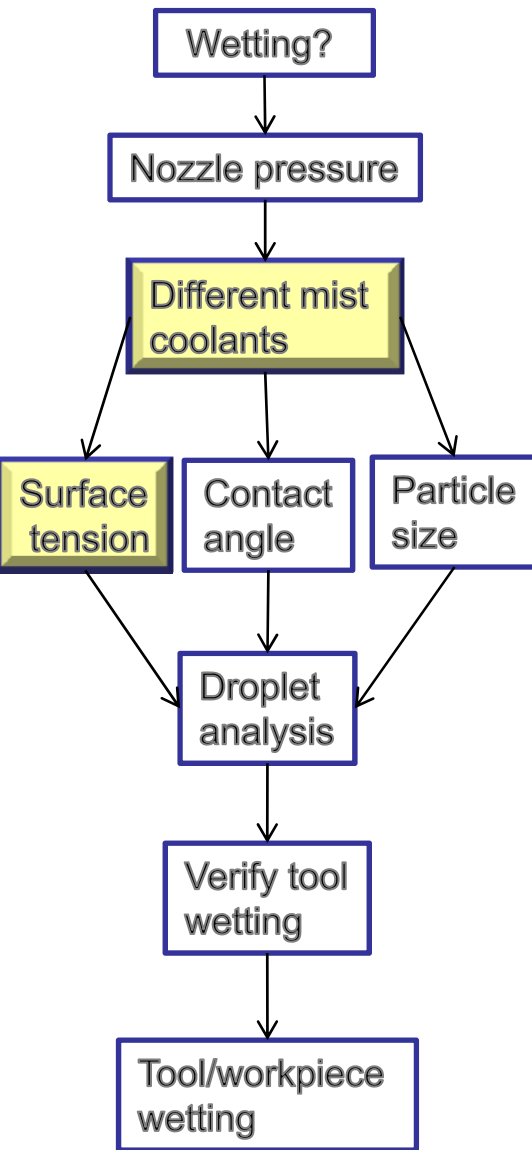
Mist nozzle

Steel Sheet





MACHINING: micromist



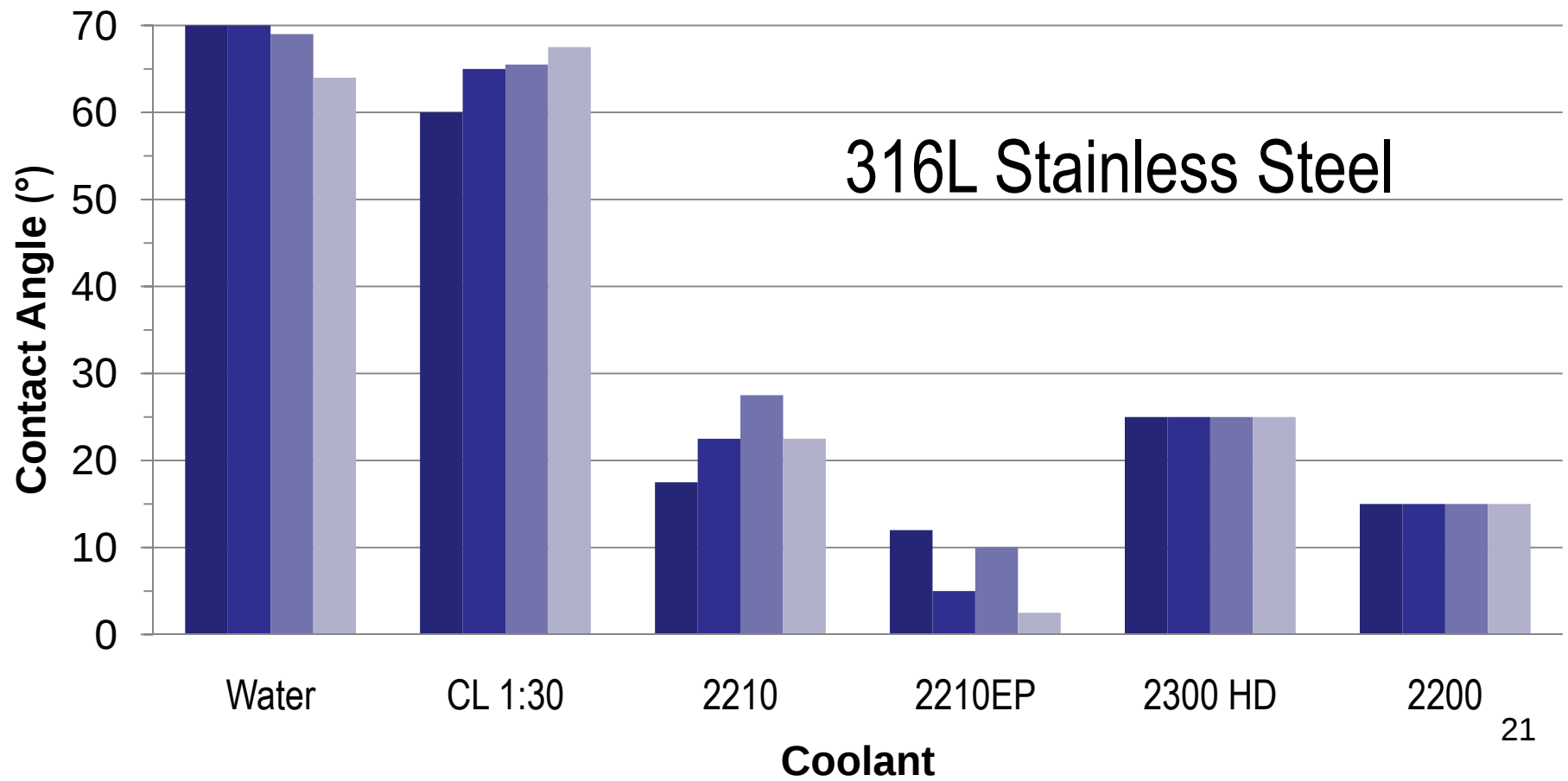
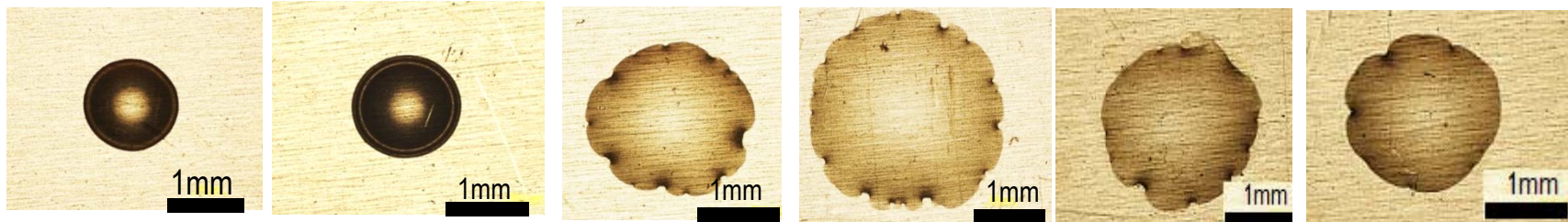
Apparatus for Surface tension measurement

1. Needle for delivering liquid droplets

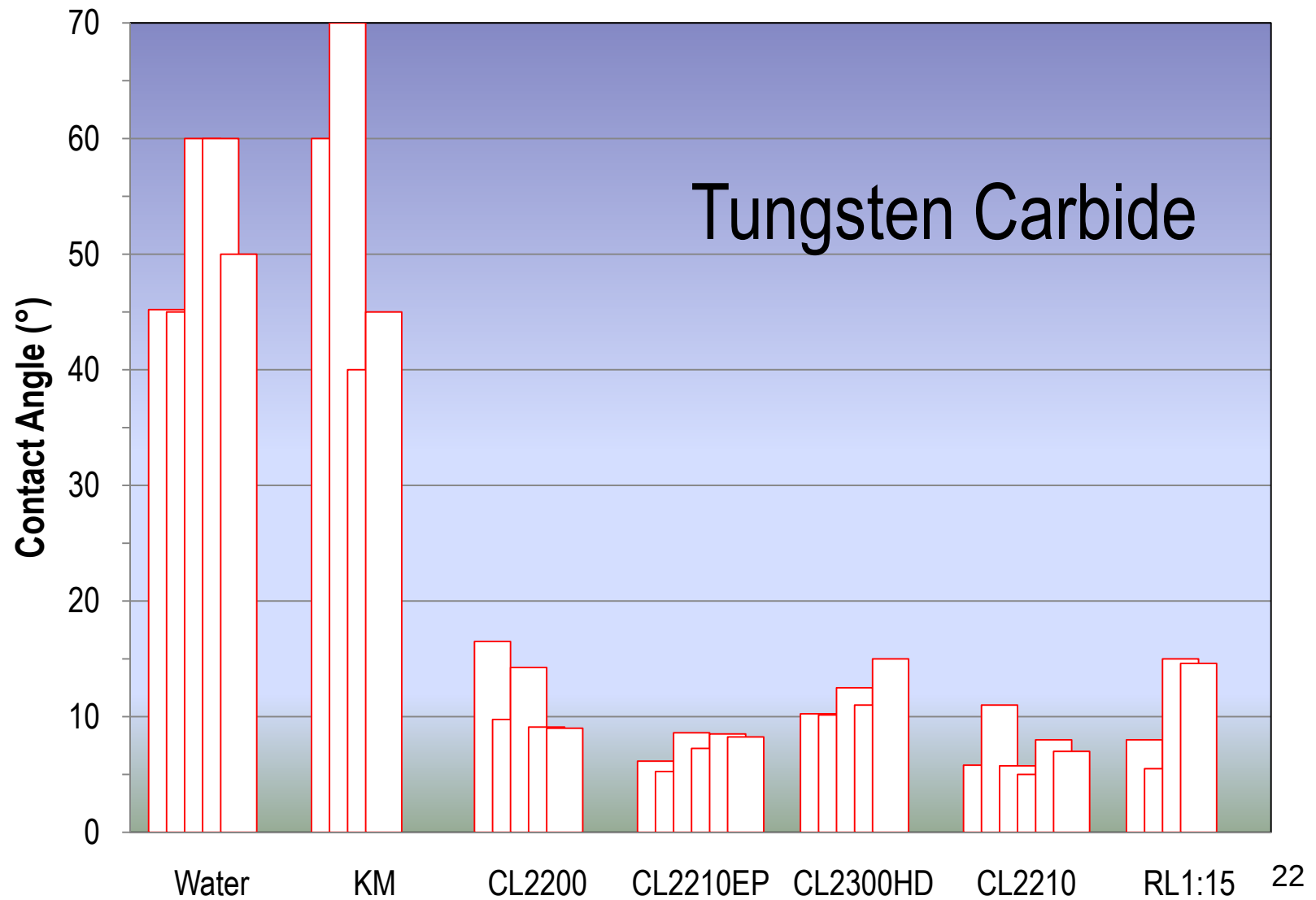
2. Camera

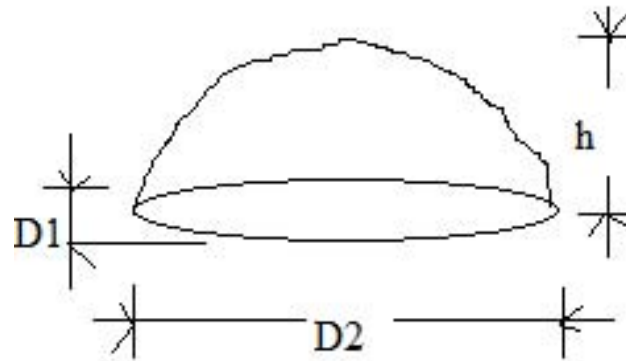
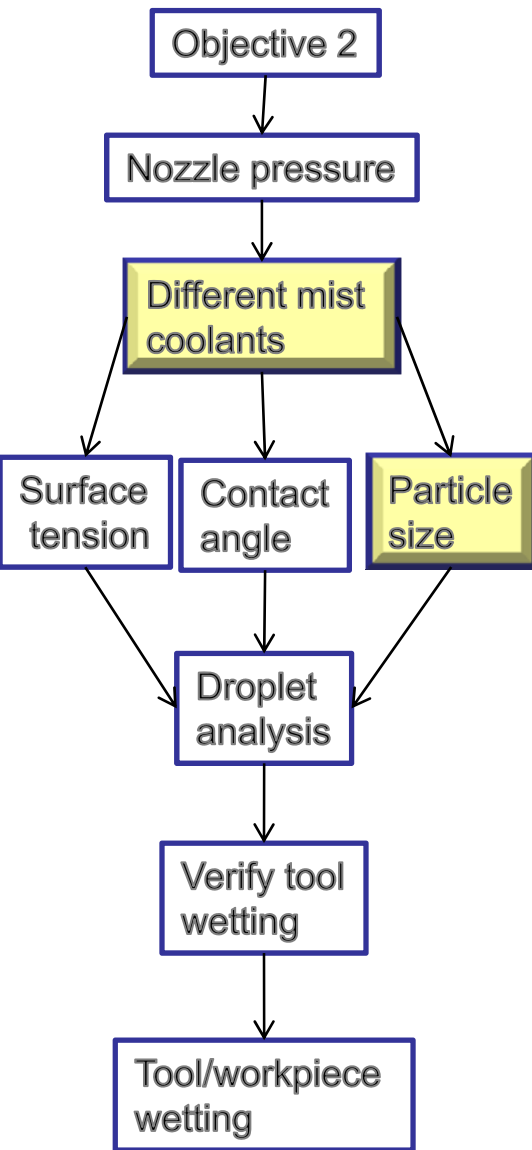


MACHINING: micromist



MACHINING: micromist





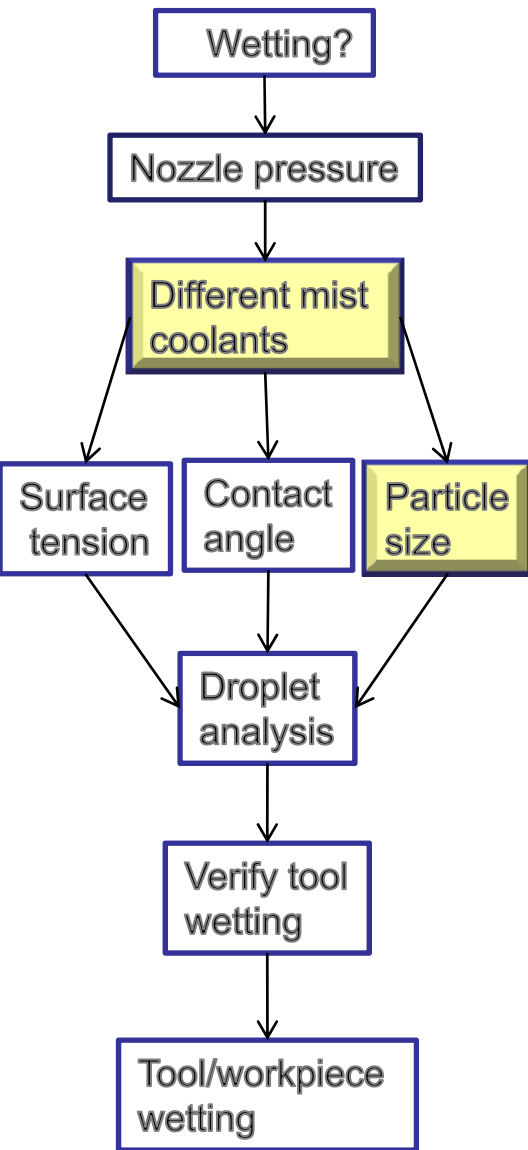
$$V = \pi h^2 \left[\frac{h}{6} + \frac{r^2}{2h} \right]$$

$$V = \frac{4}{3} \pi R^3$$

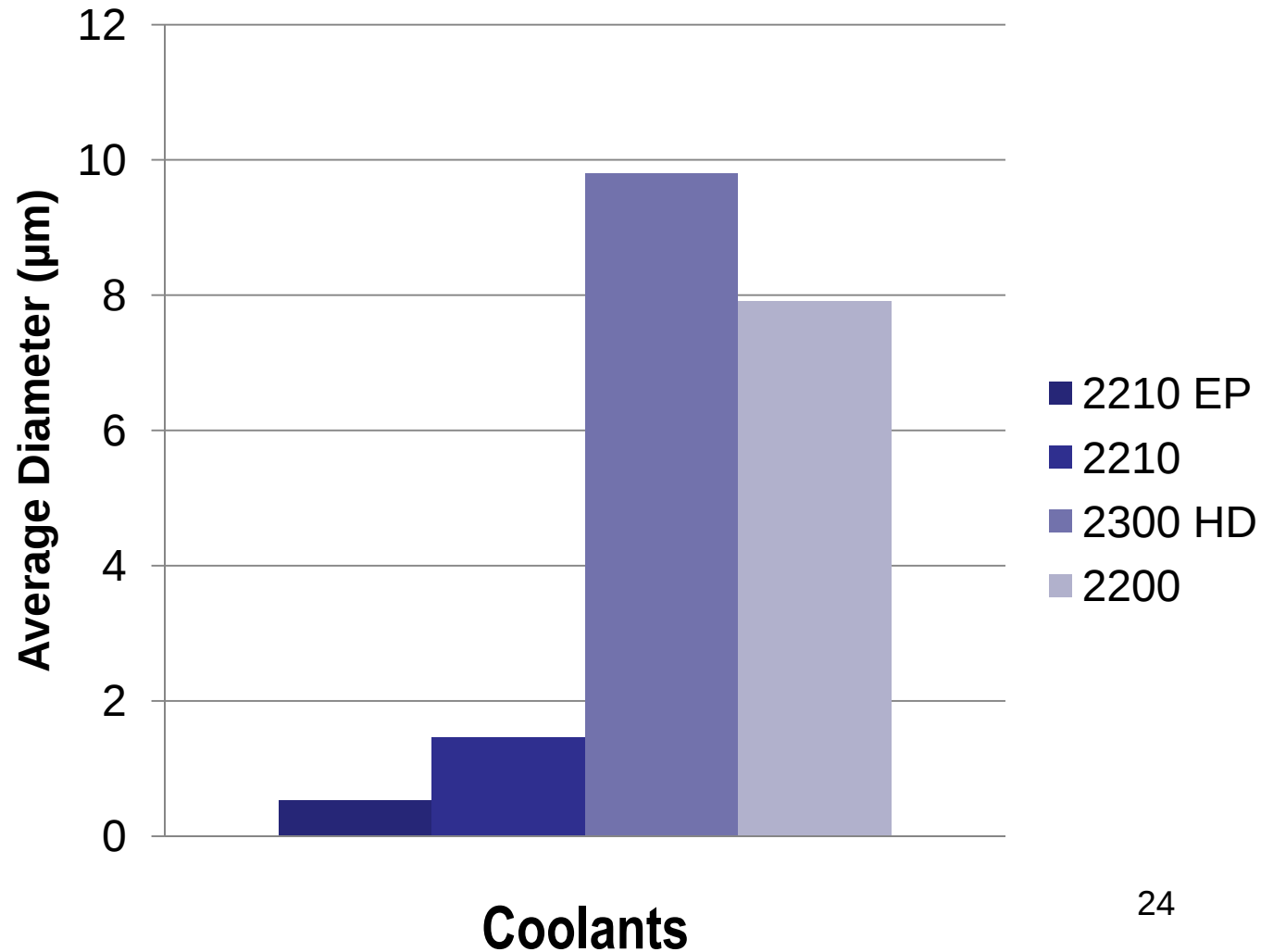
V: volume of droplet
 h: height of droplet
 R: radius of airborne droplet
 r: $(D_1 + D_2)/4$

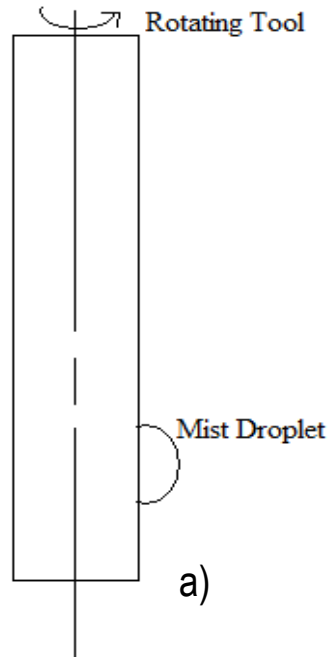
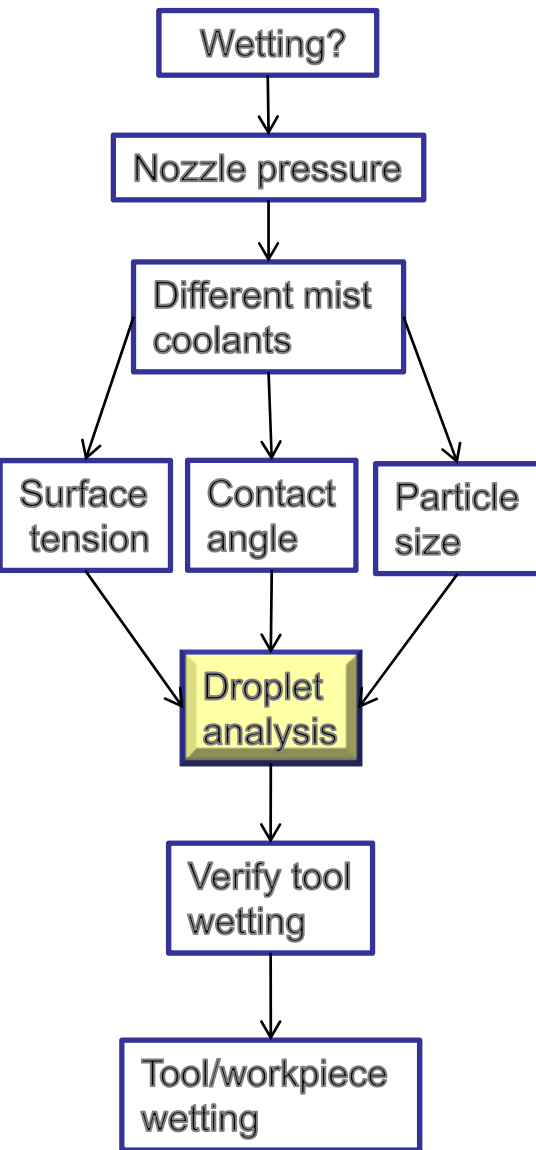


MACHINING: micromist

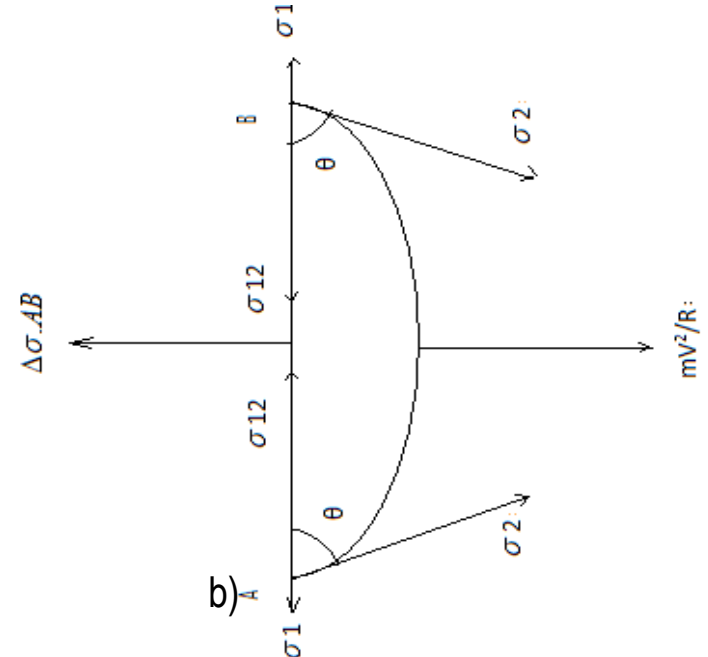


Coolant drop size comparison





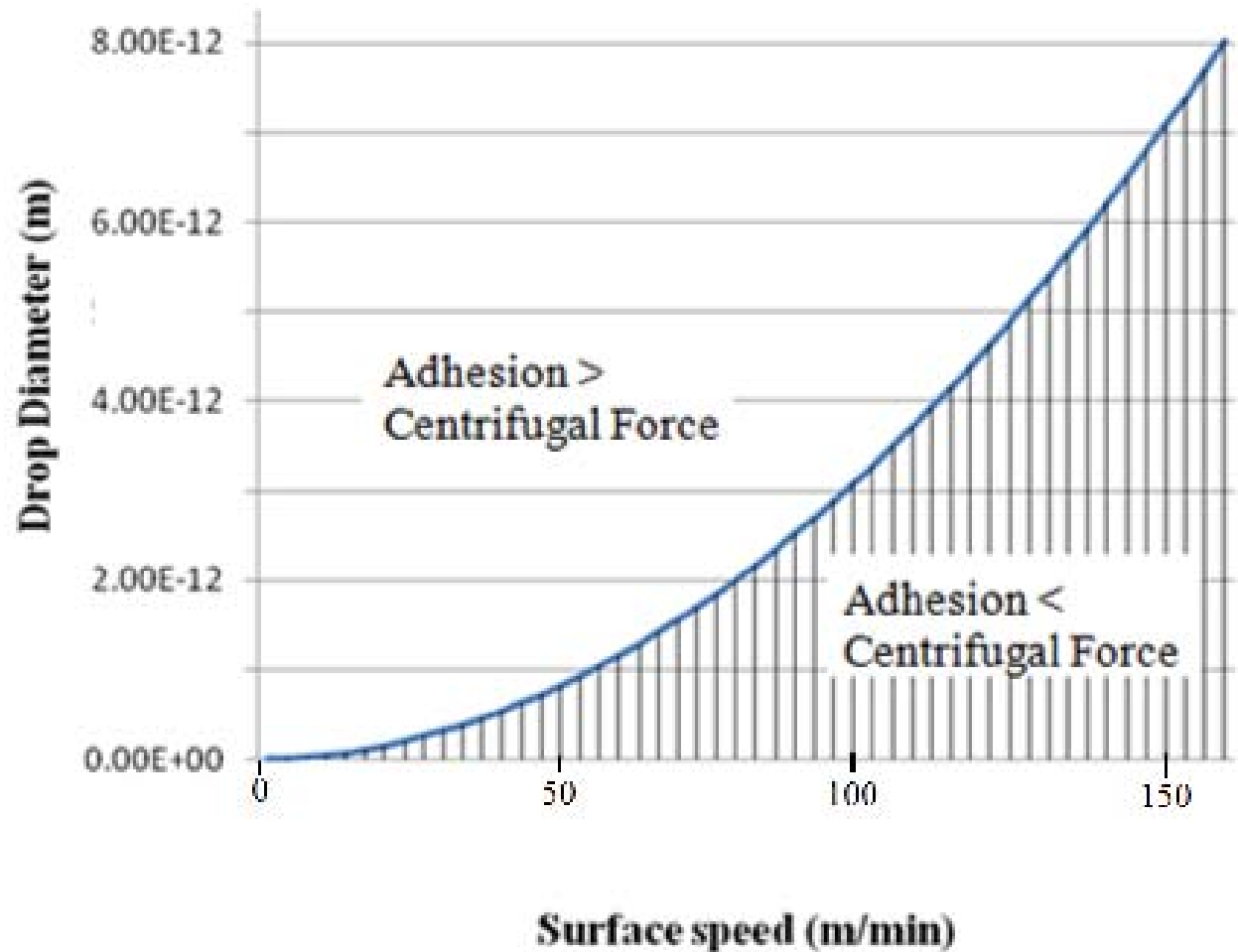
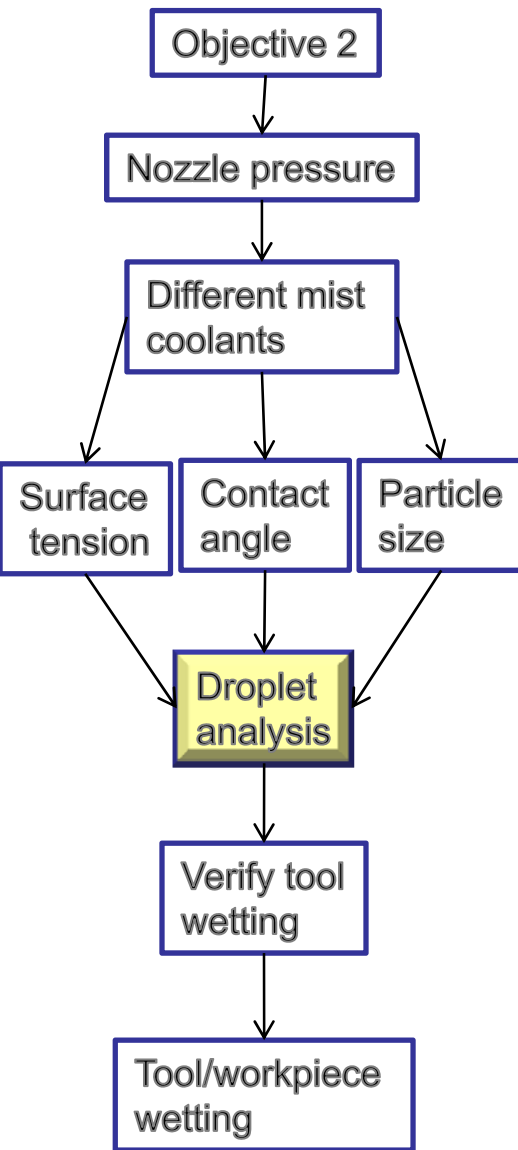
(a) Micro-droplet on a rotating tool;



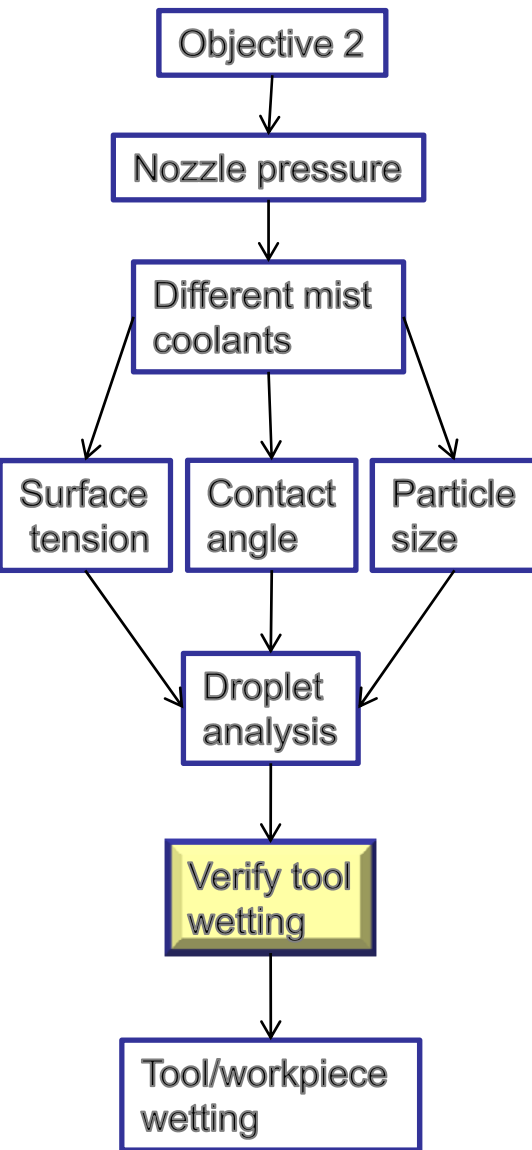
(b) Free body diagram of forces acting on the micro-droplet

$$\frac{mv^2}{R} + 2 \sigma_2 \sin \theta = \Delta \sigma D$$

m: mass of droplet
 v: surface speed of tool
 R: radius of tool
 D: diameter of droplet
 σ_2 : surface tension of liquid



Balance of adhesion and centrifugal force on a 2210EP microdroplet



Parameters of tool wetting experiments:

- Tools are run from 0-500 m/min
- Tool diameter: 3.175mm, 12.7mm
- Air pressure: 3.197 to 3.39 bar
- Stroke length: 2.7 mm
- Stroke frequency: 12 strokes/min
- Volume flow rate of coolant: $3.33 \times 10^{-9} \text{ mm}^3/\text{sec}$

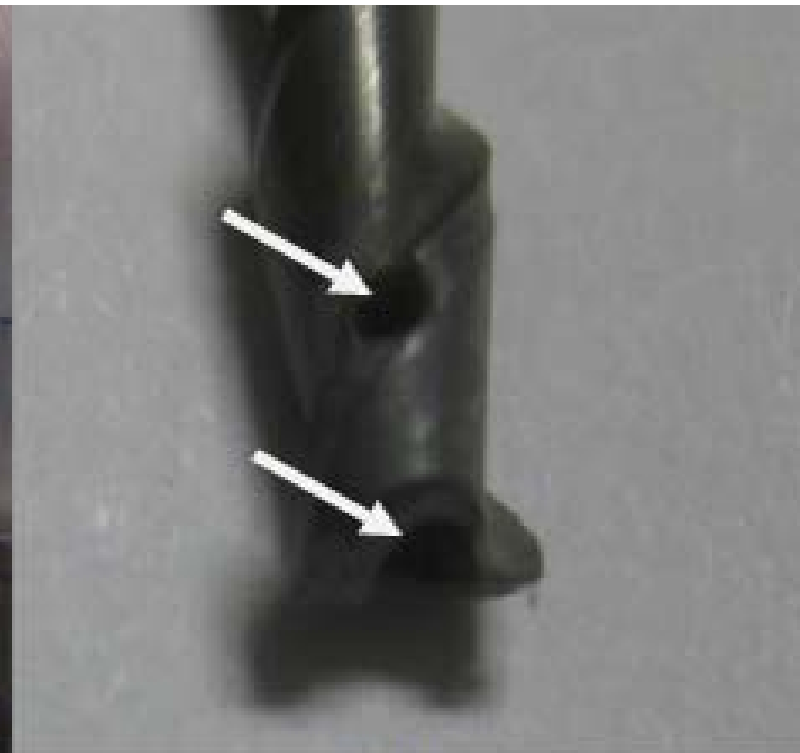


APPROACH – OBJECTIVE # 2

Setup for validation of tool wetting



(a)



(b)

(a) Mist spray setup (b) 3.175 mm 2 flute end-mill
12.7mm 2 flute end-mill (not shown)



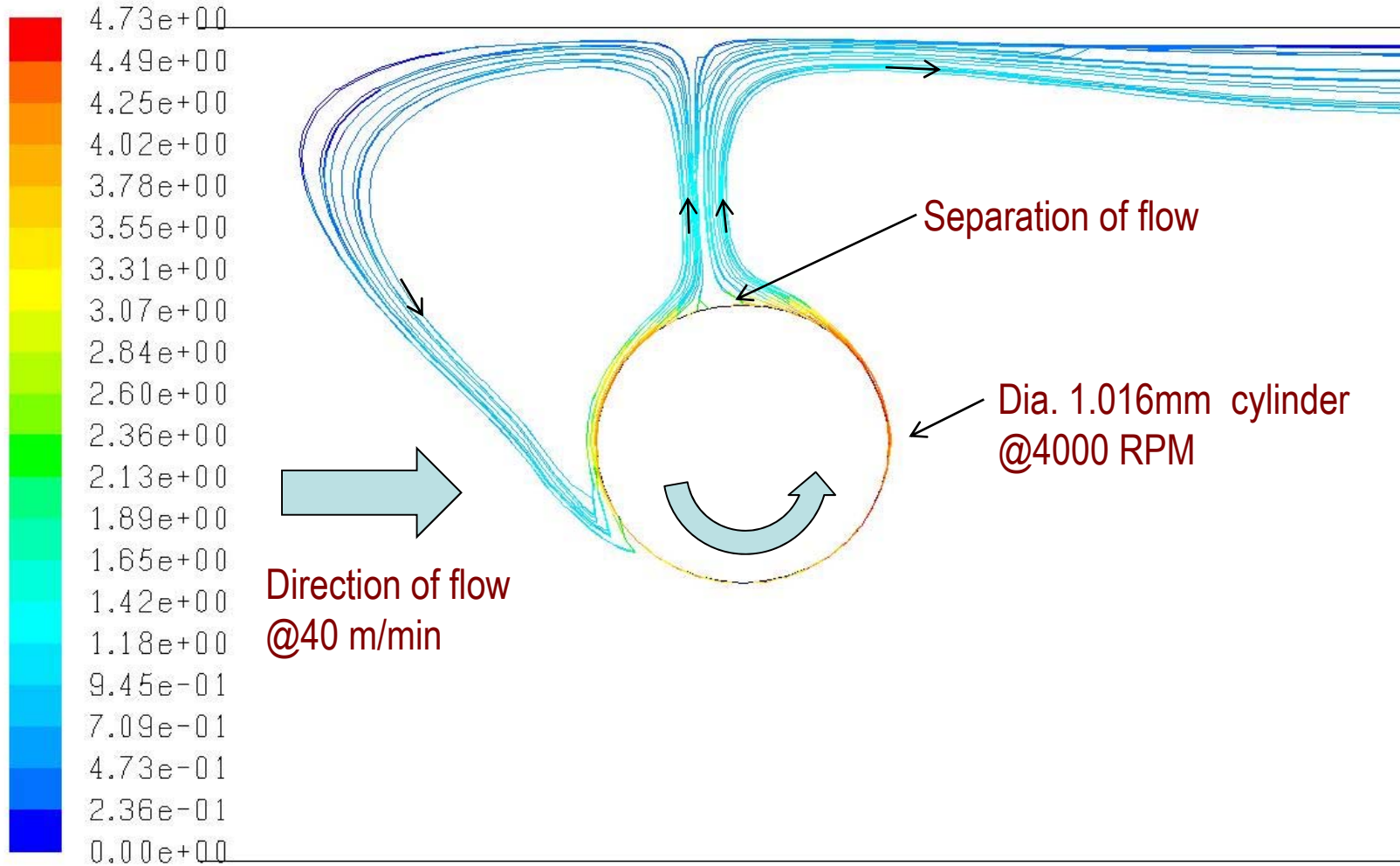
RESULT: flow of micromist

Flow?

Particle trajectory

CFD modeling

Optimal tool/workpiece/
nozzle positions

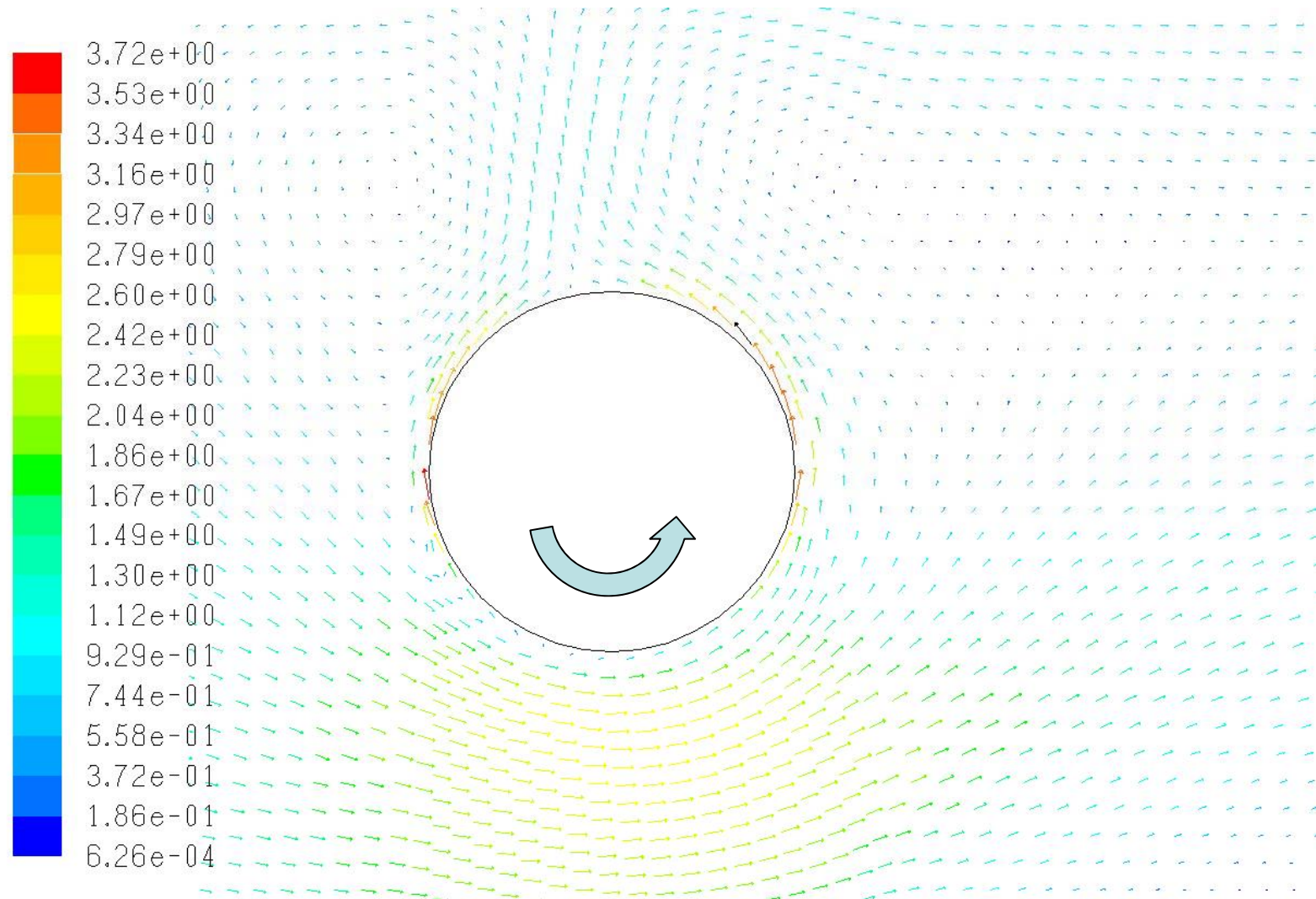


Pathlines Colored by Velocity Magnitude (m/s)

Nov 11, 2008
FLUENT 6.3 (2d, pbns, lam)



RESULT: flow of micromist



Velocity Vectors Colored By Velocity Magnitude (m/s)

Nov 11, 2008
FLUENT 6.3 (2d, pbns, lam)

Flow?

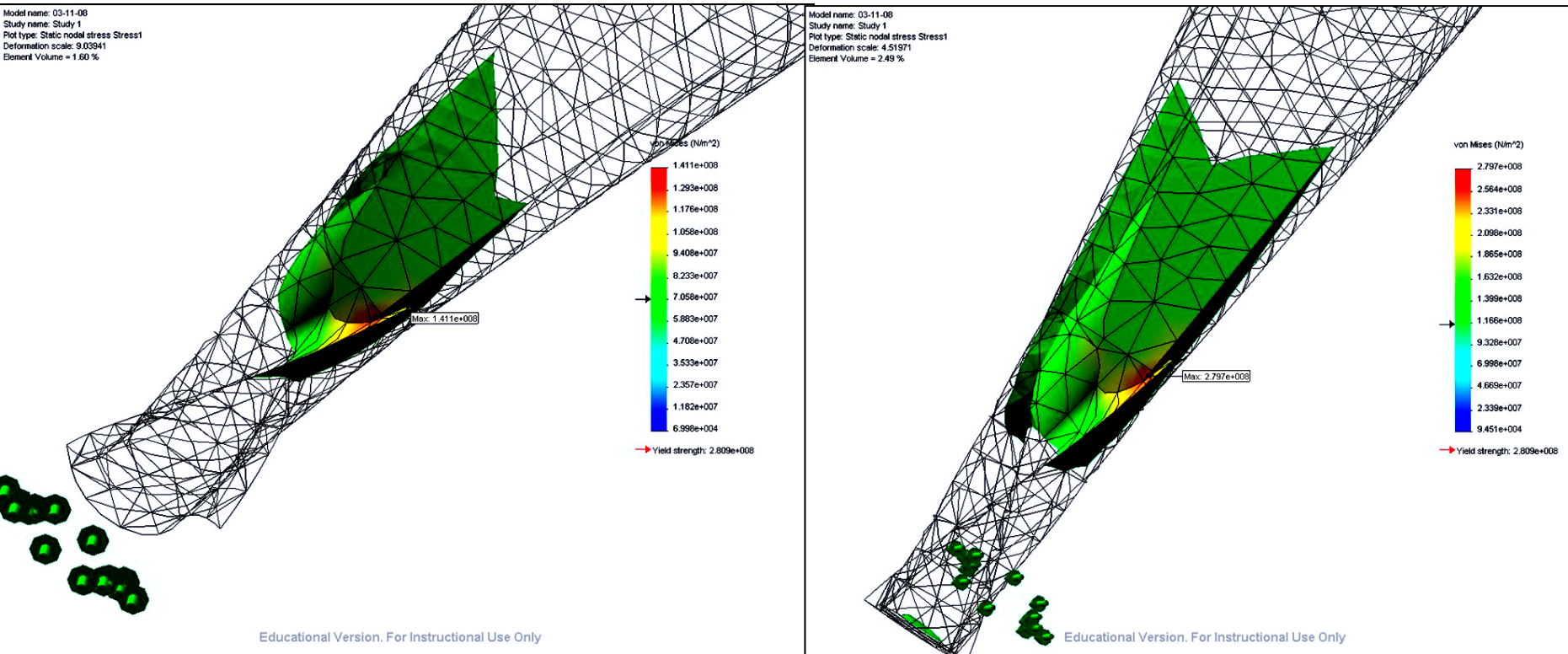
Particle
trajectory

CFD
modeling

Optimal
tool/workpiece/
nozzle positions

MICROMACHINING: tool deflection

Spindle runout, built-up edge, uncontrolled chip, and/or cutting force deflect a microtool cyclically and cause premature tool failure.

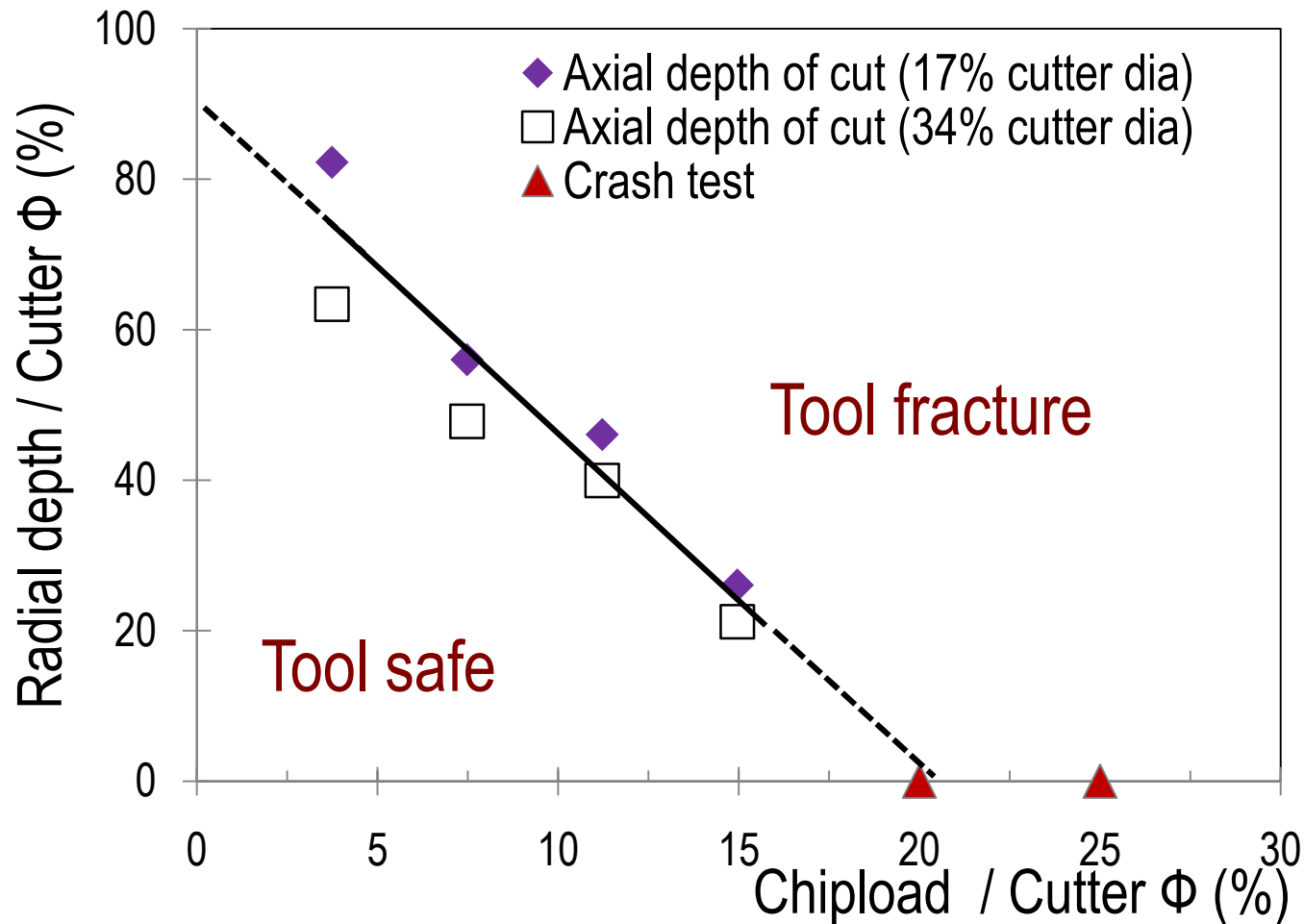


End deflection=17% tool diameter
Bending stress= 50% tool strength

End deflection=34% tool diameter
Bending stress= 100% tool strength

Finite element analysis of bending stress on a micromilling tool.

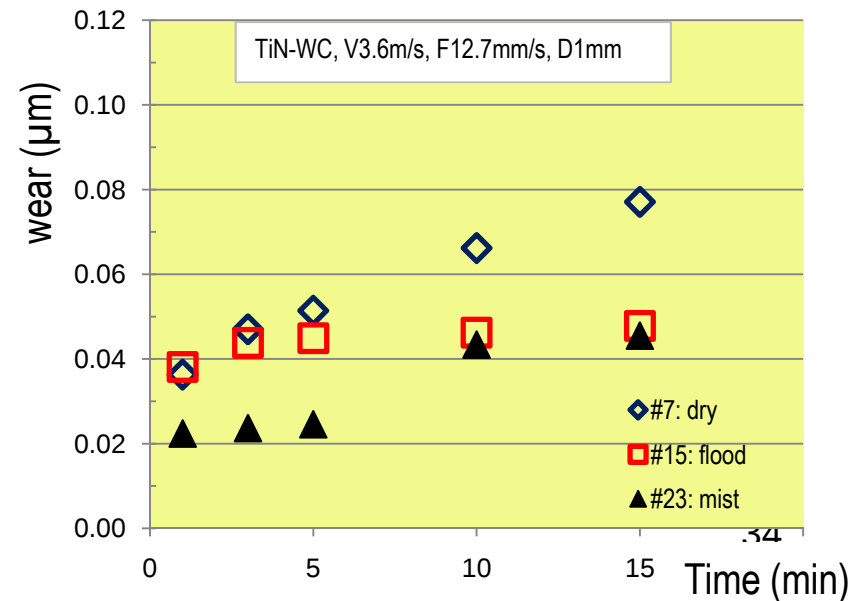
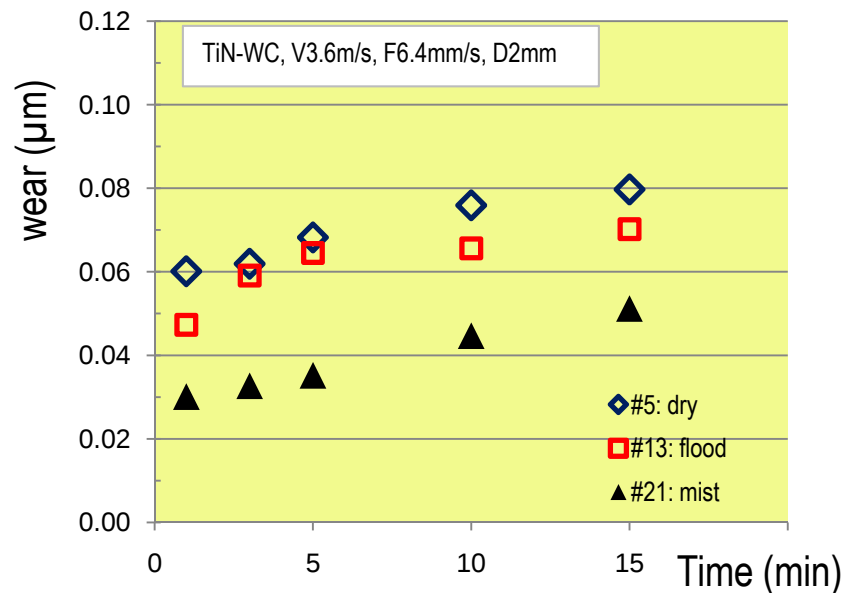
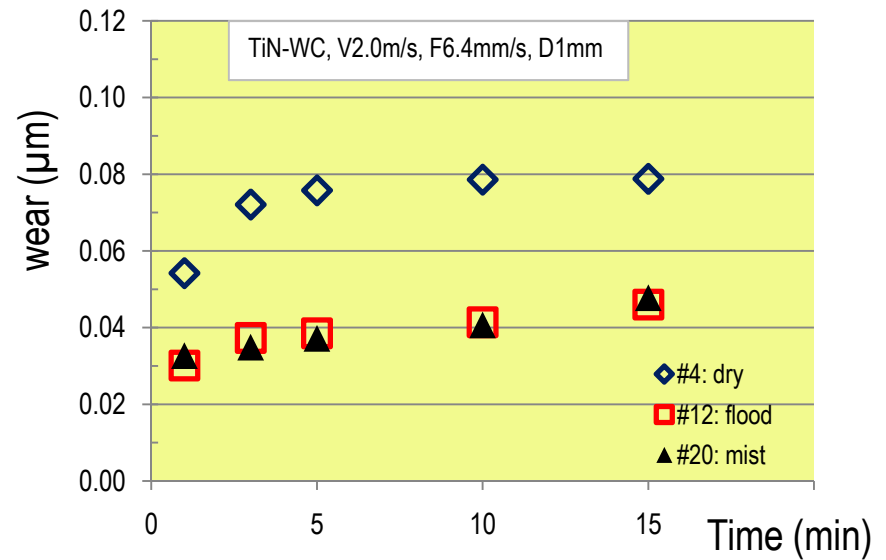
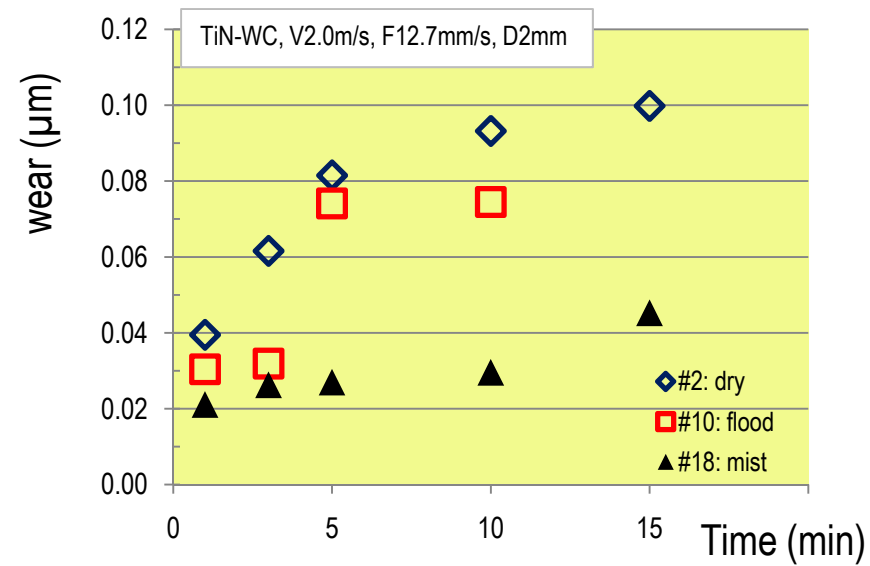
MICROMACHINING: limit of parameters



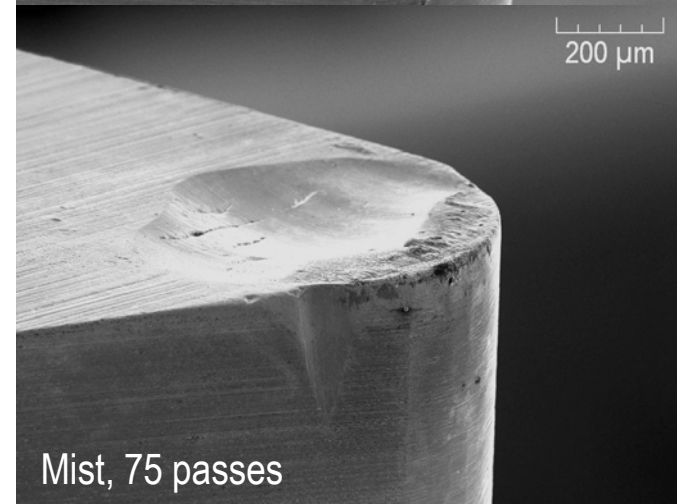
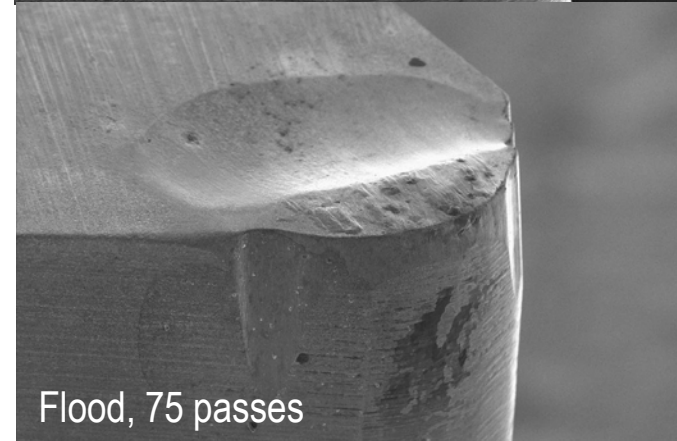
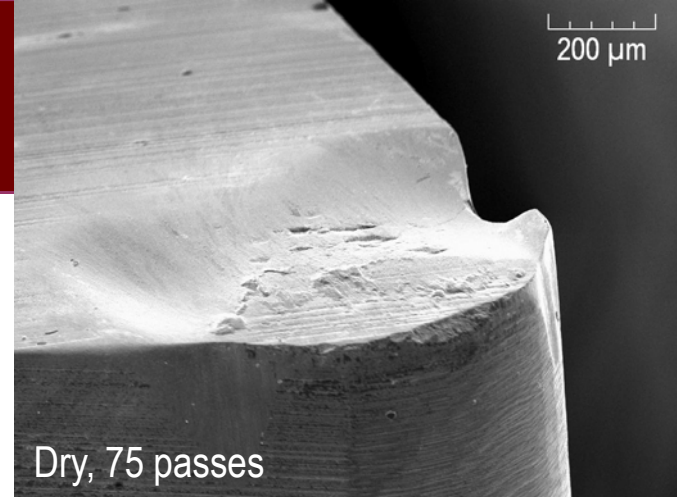
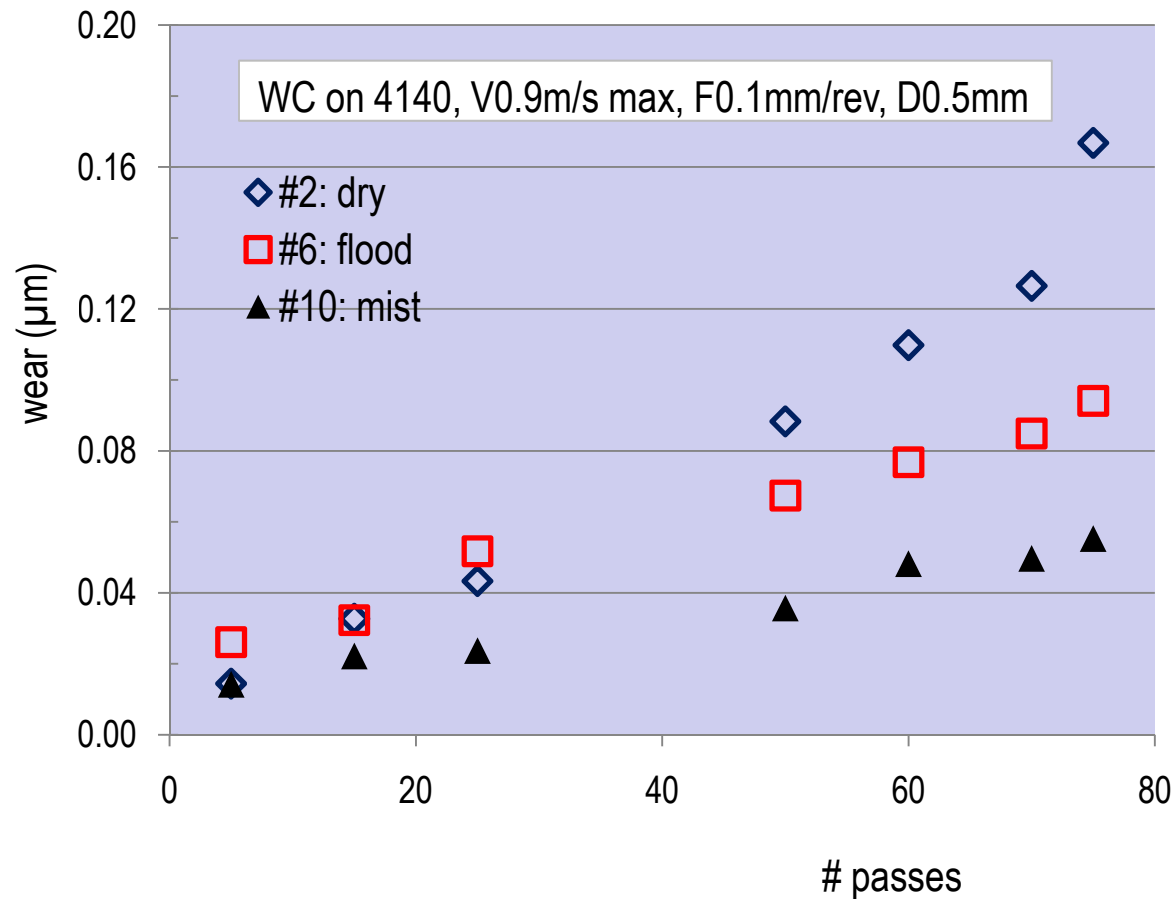
Catastrophic failure threshold of micromilling tools.

0.35mm (0.014 in) axial depth, dry, climb (down) side milling of 316L stainless steel.

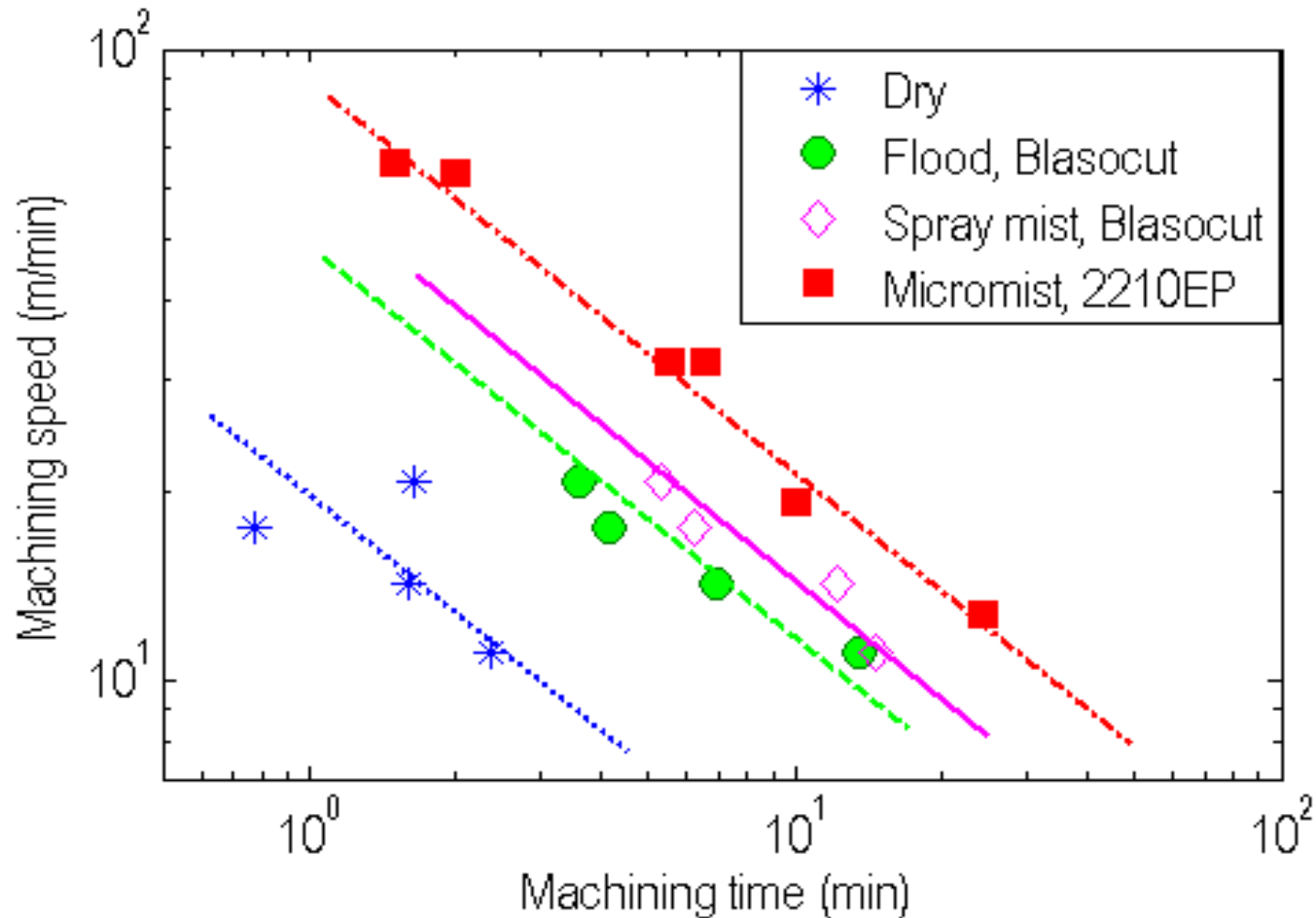
MICROMIST: macromilling



MICROMIST: macrofacing



MICROMIST: micromilling



Micromilling of 316L stainless steel and effect of cutting fluids.

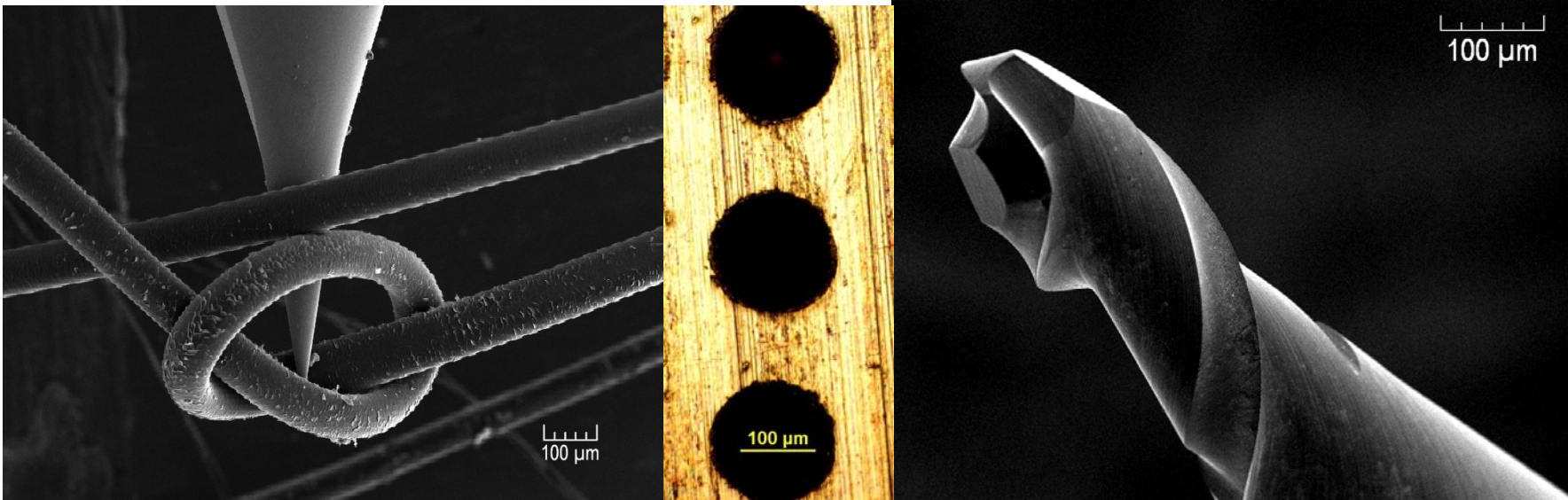
10 $\mu\text{m}/\text{tooth}$ (0.0004 in/tooth), 0.35mm (0.014 in) axial depth, 0.56 mm (0.022 in) radial depth, climb (down) side milling

MICROMIST: summary

- 1) NSF-RET program
 - Promote collaboration among schools and industry
 - Encourage college grads to continue for higher degrees
- 2) Effective micromist must:
 - Penetrate and adhere to moving tool/workpiece.
 - Wet both tool and workpiece.
 - Avoid stagnant mist location.
- 3) Optimal micromist increases tool performance
 - Macromachining.
 - Micromachining.
- 4) Submicron mist particles
 - Contaminate other equipment.
 - Pose potential health issues.
 - Should be used with air cleaner unit.

MICROMIST: future works

- 1) Complete DOE experiment and compare with theoretical data
- 2) Compare economic advantages of dry, flood, and mist
- 3) Apply to machines at TSTC Waco and BMC Athens
- 4) Extend micromilling and include microdrilling studies using tool steel, aluminum, and titanium.
- 5) Optimize tool coating





☐ National Science Foundation (NSF award #0552885).

☐ Mr. Dave Hayes, Haas Automation Inc.

☐ Mr. Joe Kueter, M.A. Ford Inc.

☐ Mr. Wally Boelkins, UNIST Inc.

☐ Mr. Patrick Anderson, PMT Inc.

